

# A Unified Curvature-driven Approach for Weathering and Hydraulic Erosion Simulation on Triangular Meshes

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**Abstract:** Erosion simulation is an important problem in the field of computer graphics. The most prominent erosion processes in nature are weathering and hydraulic erosion. Many methods address these problems but they are mostly based on height fields or volumetric data. Height fields do not allow for the simulation of complex fully 3D scenes while the volumetric data have high memory requirements. We propose a unified approach for weathering and hydraulic erosion working directly on triangular meshes which simplifies the use of the method in wide range of scenarios. We take into account the observation that the speed of erosion in nature is affected by the local shape of the eroded object. We use estimation of mean curvature to drive the speed of erosion, which results in visually plausible simulation of erosion processes. We demonstrate the results of the method on both artificial 3D models and on real data.

## 1 INTRODUCTION

Erosion is mainly perceived as the process that changes the look of the landscape over the years but it also affects smaller individual objects. In the field of computer graphics and animation, it is mainly used as a means to create realistic looking landscapes and to simulate aging effects. Many methods have addressed the simulation of different types of erosion processes, however, there are still many open problems.

Most of the existing solutions work either with volumetric data or with height fields. The height fields are very convenient for erosion simulation as they can be easily used to store large-scale terrains. The simplicity of the data structure also allows for very fast methods but it cannot be used to capture fully 3D scenes containing concave features and complex topology. On the other hand, the volumetric data structures can represent any object but it is usually at the cost of higher memory requirements and slower speed of the simulation.

As triangular meshes are by far the most commonly used object representations in computer graphics, it is reasonable to design methods using this structure. The main advantage of triangular meshes in relation to erosion simulation is their adaptivity and the possibility to model complex concave features. The triangular mesh data structure allows to model an ob-

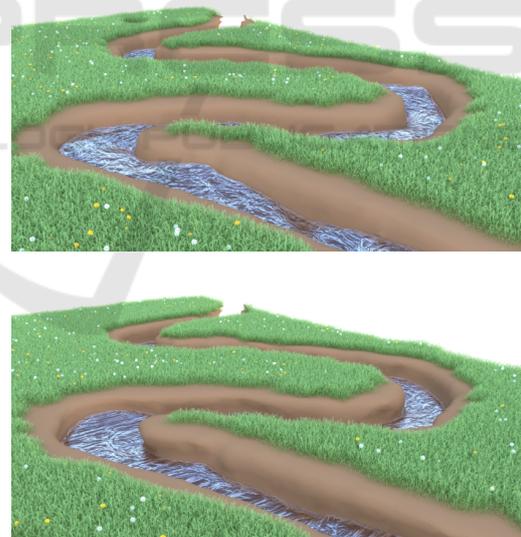


Figure 1: Running water creates undercuts on the river banks; front view. Original model (top) and the scene after 200 iterations (bottom) of hydraulic erosion simulation.

ject adaptively with varying density of vertices based on the complexity of the object, leading to lower memory requirements of the scene when compared to the volumetric approaches, while it keeps the ability to model fully 3D scenes with complex features. However, the use of triangular data structures introduces other challenges. It may be more difficult to es-

timate the object properties such as curvature on irregular data structures. Also, when the triangular mesh is being deformed during the simulation, it has to be deformed in such a manner that does not damage its integrity.

We propose a fast method that is working directly on triangular meshes and uses curvature estimation to drive the speed of erosion to simulate visually plausible erosion scenarios without using complex physically-based erosion function. The idea to use the curvature of the object to control the speed of erosion is supported by the observation of the erosion processes in real life. The areas with high mean curvature are more exposed to natural influences and are eroded at a faster rate, while the areas with zero or negative curvature are more protected and are eroded at much slower rate. We focus our efforts on spheroidal weathering and hydraulic erosion processes as these have the highest impact on the alteration of landscape elements over the years. Figure 1 shows a sample result of our hydraulic erosion simulation. The fluid represented by a particle system erodes the terrain and undercuts the river banks creating distinct overhangs especially in the river bends. The scene and erosion simulation settings will be discussed in further detail in Section 4.

To summarize, the main contributions of our paper are:

- The simulation of spheroidal weathering and hydraulic erosion is performed directly on triangular meshes.
- The simulation speed is driven by mean curvature of the model which results in highly realistic results.
- The method represents a fast unified approach that can be used to simulate both spheroidal weathering and hydraulic erosion.

The paper is organized as follows: Section 2 presents the state-of-the-art methods in the field of erosion simulation. Section 3 describes the proposed solution and Section 4 presents the results of the proposed algorithm. Finally, Section 5 concludes the paper.

## 2 RELATED WORK

Erosion is a process happening in nature by which material such as sand and rocks is taken from its original location, transported and deposited at another location by means of water, wind or other natural forces. Erosion is a long-term process that is usually studied in the context of terrain alteration where

it is the most noticeable. It can however also be observed on smaller individual objects, such as rocks and stones. The man-made objects, e.g., buildings, roads or statues, are also affected by the erosion processes. Weathering and hydraulic erosion are the two types of erosion that have the highest impact on the alteration of the landscape and as such are receiving the highest attention.

Weathering is a process of breaking down rocks, e.g., due to the contact with chemical substances, living organisms or due to thermal changes. One of the first weathering approaches was presented by Musgrave et al. (Musgrave et al., 1989). They use a simplified global erosion method to simulate weathering on a fractal terrain stored as a height field. Another weathering approach was presented by Beneš and Arriaga (Beneš and Arriaga, 2005) which was designed to generate table mountains. Dorsey et al. (Dorsey et al., 1999) presented a method for modeling and rendering of weathered stones using a novel voxel surface-aligned data structure called *slab*. This structure works as an intermediate between the stone and the surrounding erosion factors and restrains the erosion computation to the regions adjacent to the surface. Jones et al. (Jones et al., 2010) presented an algorithm for spheroidal and cavernous weathering of rocks with concave surfaces. The algorithm is built on a voxel grid and the erosion is calculated through the mean curvature estimation. Tychonievich and Jones (Tychonievich and Jones, 2010) proposed a weathering method using a tetrahedral mesh data structure based on Delaunay deformable models (DDM). They are able to generate visually plausible results, however, the method is very computationally expensive.

Hydraulic erosion is the erosion caused by still or running water, but also the erosion caused by glaciers or avalanches. It has the most noticeable impact on the evolution of the landscape. The erosion caused by rain can smooth the rocks and mountains while the streams and rivers can cause the creation of river beds, valleys or canyons. Hydraulic erosion methods can be subdivided into two categories: *physically inspired methods* and *physically based methods*.

The physically inspired methods take inspiration in natural processes but do not try to simulate them exactly. Their main purpose is to mimic the erosion impacts with as little computational effort as possible, so that the results look good without the need to simulate the exact physical erosion processes. Musgrave et al. (Musgrave et al., 1989) proposed a simple hydraulic erosion algorithm simulating rain effects on a terrain represented by a height field. Chiba et al. (Chiba et al., 1998) introduced a method based

on velocity fields of the water flow. They use particles to approximate the water volume and the erosion is evaluated when a particle collides with the terrain stored as a height field. Another height field based hydraulic erosion method was presented by Beneš and Forsbach (Beneš and Forsbach, 2002). They define the hydraulic erosion through a process consisting of four independent steps that can be repeatedly applied to achieve the desired visual effect.

The physically based methods use hydrodynamics in order to simulate the erosion processes more exactly. However, even methods from this category usually introduce some simplifications of the fluid dynamics to speed up the simulation. Shallow water simulation is a simplification of Navier-Stokes equations for the fluid dynamics that is often used for hydraulic erosion simulations. The shallow water model does not allow overlaps such as breaking waves or splashes but it is often sufficient for erosion simulations. It has been used to simulate hydraulic erosion, e.g., by Beneš (Beneš, 2007) and Mei et al. (Mei et al., 2007). A volumetric Eulerian approach is used by Beneš et al. (Beneš et al., 2006) to create a fully 3D simulation of hydraulic erosion. They represent both the eroded object and the fluid as a volumetric grid and define the erosion using processes that alter the state of the voxels of the scene. Wojtan et al. (Wojtan et al., 2007) simulate corrosion and erosion of solid objects stored as a level set and simulate the erosion by advecting it inward and the deposition by advecting the level set outward. Other methods use Lagrangian approach and describe the fluid using a particle system. Krištof et al. (Krištof et al., 2009) use the particle-based Smoothed particle hydrodynamics (SPH) to simulate erosion on terrains represented by a height field. They represent the water flow with the SPH particles that erode the terrain on collision. Later, Crespín et al. (Crespín et al., 2014) extended the method by representing the terrain as a 3D generalized map (Lienhardt, 1994). A similar SPH-based approach is used by Skorkovská et al. (Skorkovská et al., 2015) to simulate hydraulic erosion on terrains represented using triangular meshes.

The most recent methods focus on automated generation of large visually plausible landscapes. Cordonnier et al. (Cordonnier et al., 2016) presented a method that combines tectonic uplift and hydraulic erosion to achieve realistic-looking terrains. Later, Cordonnier et al. (Cordonnier et al., 2017) extended the method to take into account the vegetation and simulate the mutual impact between the vegetation and the terrain erosion during the evolution of the landscape.

However, none of the aforementioned methods al-

lows for the simulation of erosion on small-scale but complex fully 3D objects that would have sufficient quality and at the same time was not very computationally expensive.

### 3 PROPOSED SOLUTION

The proposed approach simulates erosion on objects represented as triangular meshes and uses curvature to control the degree of erosion at different parts of the eroded object. The erosion is then simulated by using vertex displacement in the direction given by the vertex normal and the discrete Laplace-Beltrami operator.

#### 3.1 Curvature Estimation

Curvature is a surface property that describes how bent a surface is at a given point. As the proposed method works on discrete triangular meshes, the curvature cannot be calculated exactly and has to be estimated. There are many methods that can be used to estimate curvature on triangular meshes; for a thorough survey, the reader can refer to the paper by Váša et al. (Váša et al., 2016). We have used the curvature estimation as proposed by Rusinkiewicz (Rusinkiewicz, 2004) due to its simplicity and performance. However, any other curvature estimator could be used in its place as we only need the curvature to capture the rough shape of the eroded object.

We use mean curvature  $H$  in our simulation as its values correspond to the region types important for erosion; the mean curvature is negative in concave regions (valleys, gaps), zero in flat areas and positive in convex areas (hills). In the rest of the paper, we will use the curvature color coding as depicted in Figure 2; negative mean curvature is represented by blue color, zero mean curvature by green color and positive mean curvature by red color. As the curvature value is scale-dependent, we downscale the curvature value interval for each eroded object to fit in the interval  $\langle -1, 1 \rangle$ . To preserve the zero curvature areas, we find value

$$H = \max(|H_{min}|, |H_{max}|) \quad (1)$$

and scale interval  $\langle -H, H \rangle$  to interval  $\langle -1, 1 \rangle$ .

We do not alter the curvature values for scenes where the curvature interval already fits inside the interval  $\langle -1, 1 \rangle$ , as it could cause problems in scenes with almost no curvature.

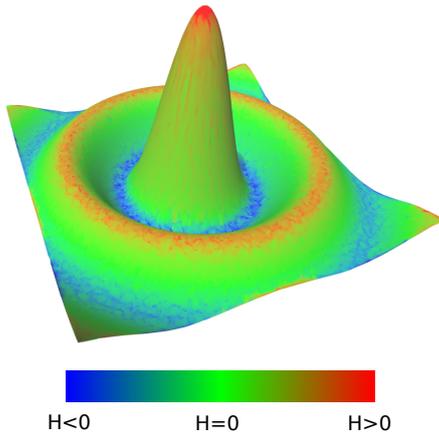


Figure 2: Curvature color coding. Negative mean curvature is represented by blue color, zero mean curvature by green color and positive mean curvature by red color.

### 3.2 Vertex Displacement

We use the mean curvature value to estimate the desired magnitude of the erosion at the given vertex of the mesh. To estimate the direction of the vertex displacement, we use the vertex normal direction and the discretization of the Laplace-Beltrami operator.

We use the uniform discretization of the Laplace-Beltrami operator, which assigns a vector  $\mathbf{L}_i$  to each vertex  $\mathbf{v}_i$ , such that

$$\mathbf{L}_i = \frac{1}{\|N(i)\|} \sum_{j \in N(i)} (\mathbf{v}_j - \mathbf{v}_i), \quad (2)$$

where  $N(i)$  is the set of vertices in the one-ring neighborhood of the  $i$ -th vertex. The resulting vectors  $\mathbf{L}_i$  capture the tangential and normal offset of the vertex  $\mathbf{v}_i$  from the average of its neighbors. In Figure 3, the vector  $\mathbf{L}_i$  represents the uniform discretization of the Laplace-Beltrami operator, the vector  $\mathbf{N}_i$  represents the normal offset and the vector  $\mathbf{T}_i$  represents the tangential offset.

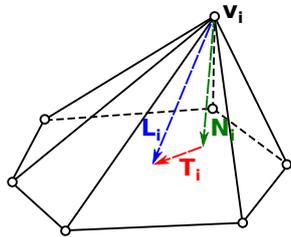


Figure 3: Uniform discretization of Laplace-Beltrami operator.

As the uniform discretization of the Laplace-Beltrami operator captures also the tangential offset, it tends to regularize the distribution of the mesh vertices. While this behavior can be undesirable in many

applications, it very well suits the needs of the erosion simulation on triangular meshes in the regions of high positive or negative curvature.

The vertex displacement can generally cause the creation of small and badly shaped triangles if the direction of the displacement is not chosen carefully. The uniform discretization of the Laplace-Beltrami operator and its ability to regularize the vertex distribution alleviates the problem and results in formation of more even triangles. Figure 4 captures the difference between results of the erosion simulation of a cube when uniform discretization of the Laplace-Beltrami operator and the opposite direction of the vertex normal is used for the vertex displacement direction. The left image shows the original mesh, the center image shows the results of the simulation after 100 steps if the Laplace-Beltrami operator is used for the vertex displacement direction, and the right image shows the corresponding results if vertex normal is used instead. It can be seen that the use of the uniform discretization of the Laplace-Beltrami operator results in more regular and nicely shaped triangles.

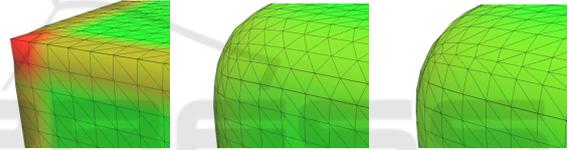


Figure 4: Direction of vertex displacement. Original mesh (left) after 100 simulation steps using the uniform discretization of the Laplace-Beltrami operator as displacement direction (center) vs. the displacement in the opposite direction of the vertex normal (right). Using curvature color coding as described in Figure 2.

On the other hand, the displacement direction based on the uniform discretization of the Laplace-Beltrami operator can cause problematic artifacts in the regions where the mean curvature is close to zero, as the tangential shift can potentially damage the mesh. For this reason, we use the direction of the uniform discretization of the Laplace-Beltrami operator for weathering simulation where we erode only mesh regions with positive mean curvature, while for the hydraulic erosion simulation we use a combination of the two aforementioned approaches.

### 3.3 Weathering

We simulate the weathering processes by displacing the vertices in the areas with positive mean curvature in the direction given by the uniform discretization of the Laplace-Beltrami operator. The displacement magnitude has to be chosen carefully in order to assure that each step of the simulation ends with a valid mesh. If the displacement is too big, inconsistencies

can be created in the mesh. Figure 5 demonstrates the problem. If a small displacement step is applied, we achieve the desired smoothing effect of erosion. If the applied displacement is too big, the mesh can become tangled as a result.

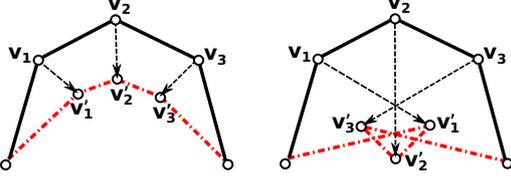


Figure 5: Small displacement step results in the desired smoothing effect (left), while too big displacement can damage the mesh (right).

To estimate a reasonable length of the displacement, we take into account the average length of the edges of the eroded mesh. The smaller the triangles of the mesh, the shorter the displacement has to be in order not to damage the mesh. We have experimentally confirmed that  $1/10$  of the average edge length is a good threshold for the maximum displacement length in a single step of the simulation. However, for some highly irregular meshes this approach can still fail and create inconsistencies in the highly detailed parts of the meshes; in such a case we detect the problem by finding the mesh self-intersections and we restart the simulation with shorter displacements per step.

For each vertex  $\mathbf{v}_i$  we calculate the corresponding displacement length  $d_i$  as follows:

$$d_i = H_i \frac{e_{avg}}{x}, \quad (3)$$

where  $H_i$  is the mean curvature at the vertex  $\mathbf{v}_i$ ,  $e_{avg}$  is the average edge length and  $x$  is the modifier that limits the maximum length of the displacement to be  $1/x$  of the average edge length  $e_{avg}$ . The position of the vertex  $\mathbf{v}_i$  at the time step  $t$  is then calculated as

$$\mathbf{v}_i^t = \mathbf{v}_i^{t-1} + d_i \mathbf{L}_i, \quad (4)$$

where  $\mathbf{L}_i$  represents the uniform discretization of the Laplace-Beltrami operator at the vertex  $\mathbf{v}_i$ .

To enhance the erosion effect in the protruding regions even more, we can use a power of the mean curvature to calculate the erosion strength. As we still want to keep the relation between the maximum vertex displacement and the average edge length, the formula for the calculation of the vertex displacement length will become

$$d_i = H_i^n \frac{e_{avg}}{x}, \quad n \in \mathbb{R}_{\geq 1}, \quad (5)$$

where  $n$  is the power modifier of the mean curvature value.

To validate the correctness of the weathering effect of the presented approach, we have applied the erosion simulation to a cube model. Figure 6 shows the original cube model and the model after 30, 100 and 200 steps. The power modifier  $n$  was set to 1 for this simulation. As can be seen in Figure 6, the algorithm converts the cube to a sphere as expected.

### 3.4 Hydraulic Erosion

We propose a similar approach to simulate hydraulic erosion. We use the particle-based simulation library Flex by Nvidia (NVIDIA, 2014) to simulate the fluid. However, as we do not rely on any specific features of the library, it could be easily exchanged for any other particle-based fluid simulation system.

To simulate the hydraulic erosion, we limit the erosion processes to the regions of the mesh that are in contact with the fluid particles. For each fluid particle that collides with the mesh, we search for all the vertices that are within the region of influence  $d_{influence}$  of the particle. In our simulations, we set the region of influence  $d_{influence}$  to be equal to the average length of the edge of the mesh, as it results in including most of the vertices of the affected triangles while excluding any vertices that are too distant from the fluid particles. To speed up the search for the close vertices, we use a simple auxiliary grid structure which stores the information about the spatial subdivision of the mesh.

As we want to have a smooth transition between the eroded and the still parts of the mesh, we calculate the distance factor  $f_{distance_i}$  of the vertex  $\mathbf{v}_i$  as follows:

$$f_{distance_i} = \frac{d_{influence} - d_{part}}{d_{influence}}, \quad (6)$$

where  $d_{part}$  is the distance between the vertex  $\mathbf{v}_i$  and the closest particle. The distance factor  $f_{distance_i}$  is then used to influence the hydraulic erosion speed as follows:

$$\mathbf{v}_{h_i}^t = \mathbf{v}_{h_i}^{t-1} + d_i f_{distance_i} \mathbf{L}_{n_i}, \quad (7)$$

where  $\mathbf{L}_{n_i}$  is the vertex displacement direction. For the displacement direction, we use a combination of the vertex normal and the uniform discretization of the Laplace-Beltrami operator. For vertices with mean curvature value of zero we use only the vertex normal, while for the vertices with mean curvature of  $H_{min}$  or  $H_{max}$  we use only the Laplace-Beltrami operator. For the remaining values, we use a linear interpolation of the vectors.

Unlike in the case of weathering, in hydraulic erosion simulation we have to be able to erode all vertices in the affected areas, regardless of their mean curvature value. The stream of water erodes flat areas as

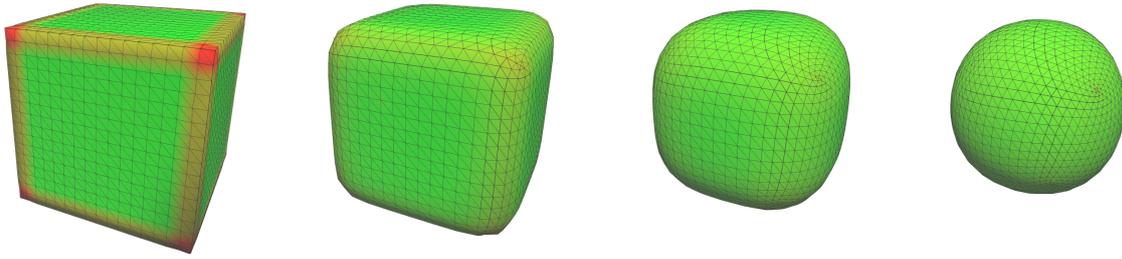


Figure 6: Validation of the weathering approach. From left to right: input cube model and the model after 30, 100 and 200 steps of the simulation. After 200 steps of the simulation, the input cube model has been eroded into a sphere. Using curvature color coding as described in Figure 2.

well as gaps and protrusions, but the speed of the erosion will differ. The strength of erosion in protruded areas is the highest, followed by flat areas and gaps. To mimic this behavior, we use a different approach for scaling the mean curvature. We scale the mean curvature value interval  $\langle H_{min}, H_{max} \rangle$  to fit in the interval  $\langle 0, 1 \rangle$ . That way, the gaps are eroded more slowly and protrusions faster, resulting in a visually plausible simulation of erosion.

## 4 RESULTS

We have performed extensive testing to demonstrate the visual quality of the results of our approach. This section presents the results of our weathering and hydraulic erosion simulation algorithms.

### 4.1 Weathering

Figure 7 shows the results of the weathering method applied on the model of the Stanford bunny (Levoy et al., 2005). The figure demonstrates the influence of the power modifier  $n$  as introduced in Equation 5. For the first row of images, the power modifier  $n = 1$ , for the second row  $n = 2$  and for the last row  $n = 3$ . Each row then represents the state of the simulation after increasing number of iterations. It can be seen that the increase of power modifier  $n$  results in slower erosion rate in the flatter regions.

The effect of the power modifier  $n$  is the most significant on models with distinct protruded regions, such as the hand model in Figure 8. The figure shows the original model (bottom rightmost subfigure) and the result of the simulation after 50 iterations with increasing power modifier. The figure demonstrates a possible problem in weathering highly protruded models if using low power modifier  $n$ . It can result in the creation of very thin features composed of very small triangles and ultimately it can cause a mesh to self-intersect.

To prevent such undesirable behavior, we improve the mesh by removing small triangles after every iteration. We used a tenth of the average edge length as a threshold for the face removal and the power modifier  $n = 5$  in the simulation captured in Figure 9. The simulation erodes the protruded finger regions in a visually plausible way.

### 4.2 Hydraulic Erosion

As mentioned before, we use the particle-based simulation library Flex by Nvidia (NVIDIA, 2014) for the fluid simulation. Figure 10 shows our hydraulic erosion method on the model of the Stanford bunny (Levoy et al., 2005). We pour the water over the bunny and simulate the hydraulic erosion using the algorithm presented in Section 3.4 only in the mesh regions affected by the water flow. This simple example shows the capability of the method to restrain the erosion to the parts of the mesh where the fluid particles collide.

We show a more realistic scene in Figure 11. The model represents a narrow canyon through which the water is poured. The simulation results in the generation of undercut cliffs around the flow of the fluid. Figure 12 compares our results to the results of Tychonievich and Jones (Tychonievich and Jones, 2010) who demonstrate their approach on a scene of similar settings. To emphasize the effect of the hydraulic erosion simulation, we do not apply any deformation to the regions of the mesh that are not in direct contact with the fluid. This results in unnaturally flat looking side walls of the model; this could be improved by adding small amount of noise to the mesh vertices.

Our next example shows the hydraulic erosion simulation on real data of a river in the Northern Moravia in the Czech Republic; the region is showed on the map cut-out in Figure 13. The data were acquired by lidar scanning and preprocessed by removing the vegetation and performing point reduction and afterwards triangulated using delaunay triangulation. However, the data have very bad quality especially in

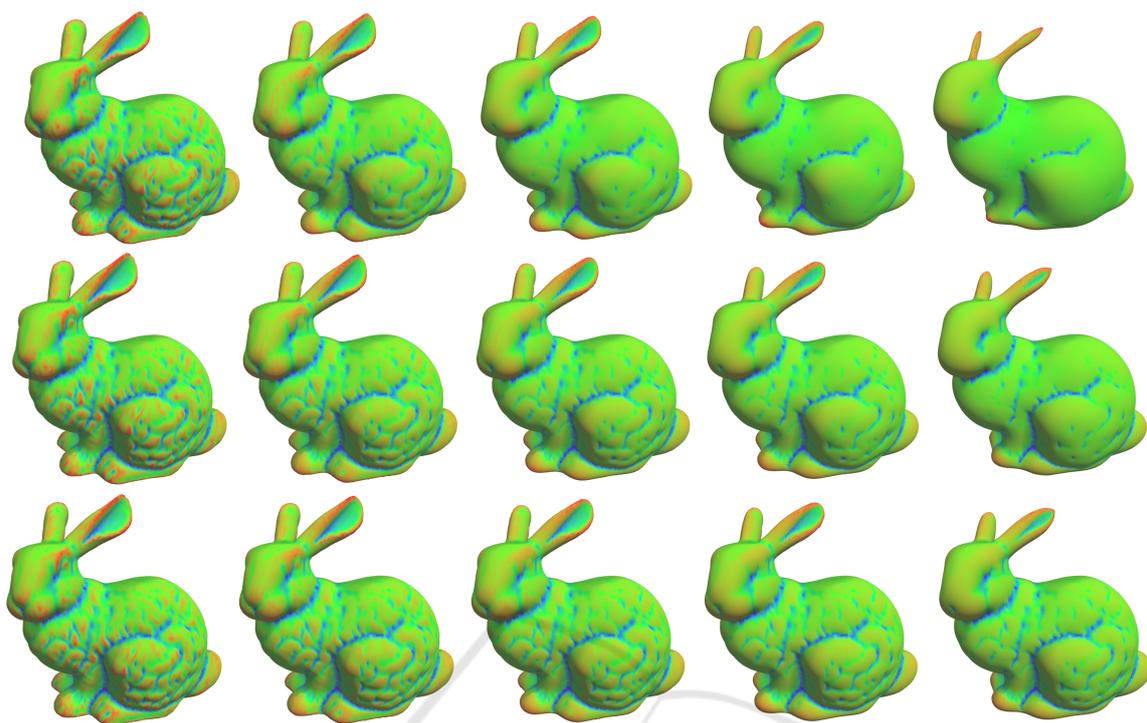


Figure 7: Influence of the power modifier  $n$ . Top to bottom: power modifier  $n = 1$ ,  $n = 2$  and  $n = 3$ . Left to right: original model, simulation after 20, 50, 100, and 200 iterations. Using curvature color coding as described in Figure 2.



Figure 8: Influence of the power modifier  $n$  on a highly protruded model. Top to bottom, left to right: original model, simulation after 50 iterations with power modifier  $n = 1$ ,  $n = 2$ ,  $n = 3$ ,  $n = 4$ ,  $n = 5$ ,  $n = 10$  and  $n = 20$ . Using curvature color coding as described in Figure 2.

the river region that is of our interest, as the lidar scanning is incapable of scanning surfaces under water. For that reason, we performed further preprocessing

using the MeshLab software (Cignoni et al., 2008). We lowered the triangles representing the bottom of the river to create the river bed. Afterwards we used

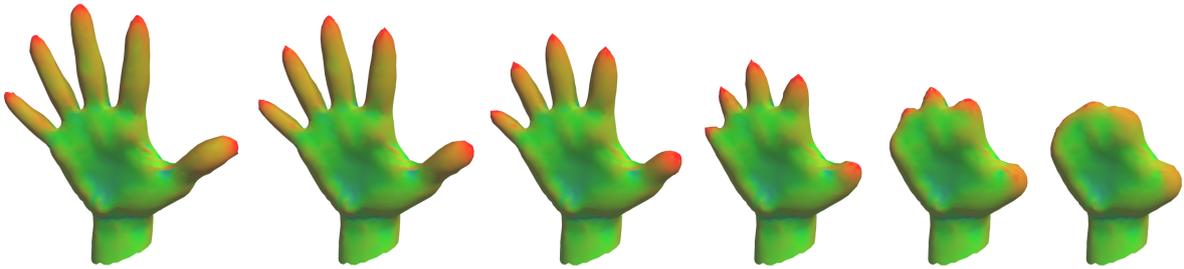


Figure 9: Weathering of a highly protruded model. Small faces are removed to prevent damaging the mesh. Left to right: simulation after 20, 50, 100, 200, 300, and 400 iterations. Power modifier  $n = 5$ ; using curvature color coding as described in Figure 2.

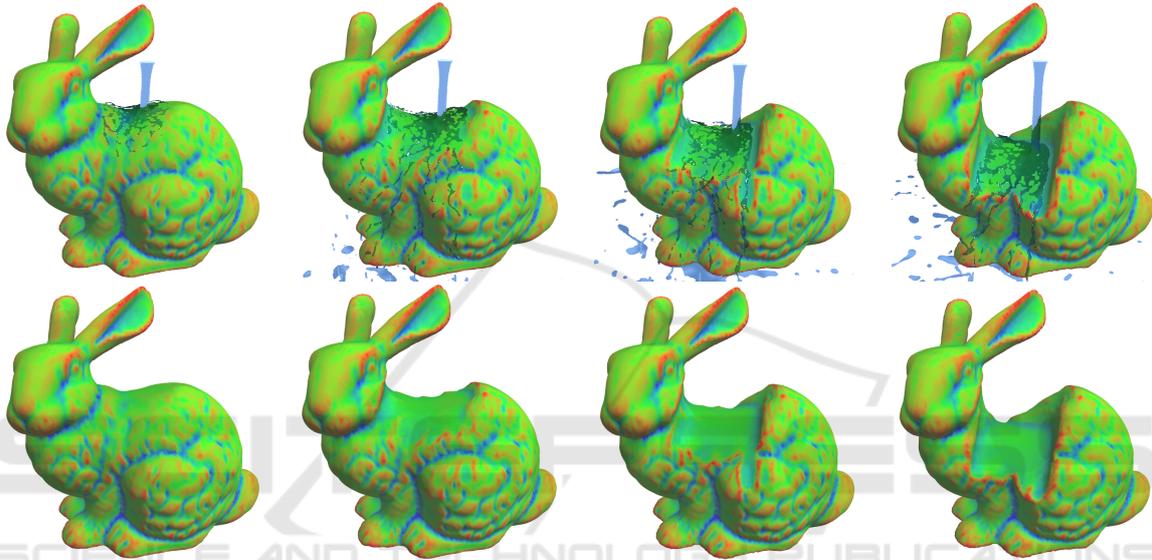


Figure 10: Hydraulic erosion simulation. Top: scene with simulated fluid; bottom: isolated model. Left to right: model after 40, 200, 400, and 700 iterations. Using curvature color coding as described in Figure 2.

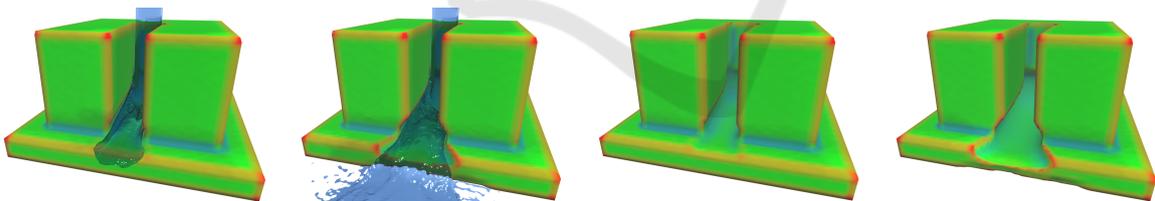


Figure 11: Pouring water through a narrow canyon. Left to right: scene with simulated fluid after 100 and 150 iterations, isolated model after 100 and 150 iterations. Using curvature color coding as described in Figure 2.

uniform mesh resampling followed by quadric edge collapse decimation. Figure 14 captures both the original triangulation and the data after preprocessing.

We simulated the process of creation of the undercuts in the river banks in the hydraulic erosion scenario captured in Figure 1. We simulated the erosion using the approach described in Section 3.4. The scene was set up with the following parameters: the power modifier  $n = 1$  and the region of influence  $d_{influence}$  of a particle was set to the average edge length. The simulation results in the creation of underdetermined river banks with distinct overhangs espe-

cially in the river bend regions, as demonstrated in Figure 1 and Figure 15.

We used the same data to simulate the flooding of the area due to high amount of fast flowing water in the river. The scene was set up with the following parameters: the power modifier  $n = 1$  and the region of influence  $d_{influence}$  of a particle was set to triple the average edge length. The increased region of influence  $d_{influence}$  results in smoothing the edges of the river bed and creating more convincing results. Figures 16 and 17 show the original scene and the result of the simulation after 100, 200 and 300 iterations.

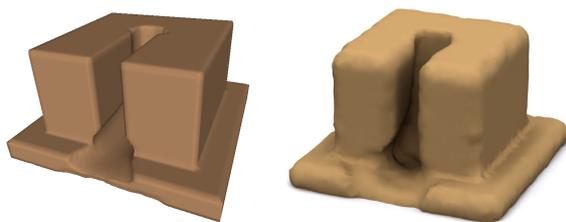


Figure 12: Pouring water through a narrow canyon. Left: our approach; right: approach by Tychonievich and Jones (Tychonievich and Jones, 2010).



Figure 13: River Odra in the Northern Moravia in the Czech Republic. Source: www.Mapy.cz.

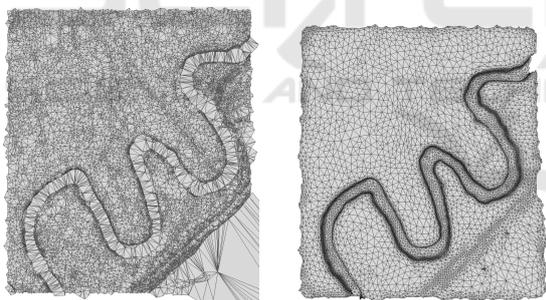


Figure 14: Triangulated lidar data (left) and the data after preprocessing (right) of a river region captured in Figure 13.

Figure 18 captures the mean curvature of the original scene and the final scene after 300 iterations.

### 4.3 Execution Time

We have measured the execution time for the scenarios presented in this Section on a computer equipped by Intel i7-4770 3.4GHz, Intel HD Graphics 4600 and 16 GB RAM. We have measured the time required per iteration of the method, as well as the execution time of the most important substeps. The measured data is shown in Tables 1 and 2 together with the number of vertices and faces of the corresponding scenes. For hydraulic erosion scenarios captured in Table 2

we also record the average number of particles in the scene. Even though we did not dedicate any special effort to speed up the simulation, the simulation times are very close to real-time frame rates. The real-time simulation could be achieved by using more sophisticated auxiliary structures or by implementing the method on the GPU.

## 5 CONCLUSION

We have proposed a novel unified approach for the two most prevalent erosion processes that can be observed in nature, i. e., weathering and hydraulic erosion. Our approach works directly with models represented as triangular meshes and simulates the erosion by vertex displacement in the direction of the vertex normal or the uniform discretization of the Laplace-Beltrami operator, while the magnitude of the displacement is calculated based on the local mean curvature value.

The main advantage of our approach is that it offers a unified way of simulating weathering and hydraulic erosion on triangular meshes, without the need to employ other auxiliary intermediate data structures. This allows us to use the simulation method on a wide range of readily available triangular models. Triangular meshes also permit to model complex scenes with detailed features with varying density of vertices based on the local complexity of the scene.

The use of triangular meshes and the simplicity of the proposed method lead to very fast execution time of the erosion simulation. We achieved almost interactive rates without deploying any special means to speed up the algorithm. As future work, we would like to achieve interactive simulation rates by performing the erosion calculations on the GPU.

We have demonstrated our approach on both artificial and real data and showed that our method results in the creation of visually plausible eroded models despite the use of very simple erosion simulation function. To increase the plausibility of the simulation, the erosion function could easily be replaced by more complex physically-based method. Also, as future work, we would like to allow the simulation of erosion of scenes composed of multiple materials by combining our approach with a multi-material simulation approach, such as the approach by Skorkovská and Kolingerová (Skorkovská and Kolingerová, 2016). Another obvious avenue for this work is the handling of topological changes, such as splitting the model in two due to heavy erosion.

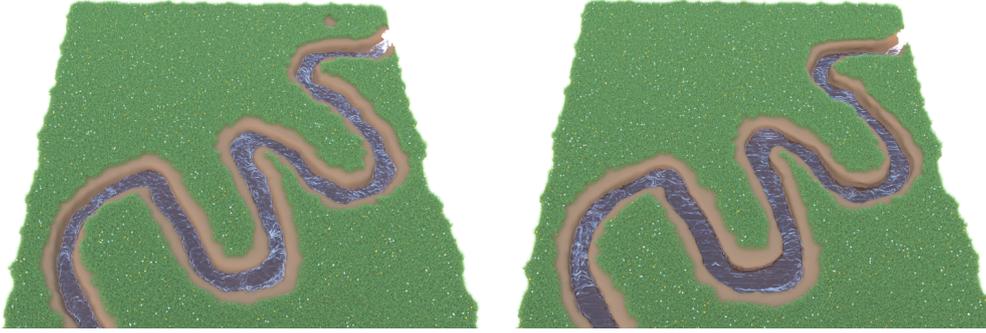


Figure 15: Running water creates undercuts on the river banks; top view. Original model (left) and the scene after 200 iterations (right) of hydraulic erosion simulation.



Figure 16: Fast water in the river erodes the river banks; top view. Top to bottom, left to right: original scene and the scene after 100, 200, and 300 iterations.

Table 1: Size of the scene and execution time of steps of the algorithm (in ms) for the weathering simulations.

	vertices	faces	iteration [ms]	curvature calculation [ms]	laplacian calculation [ms]	vertex displacement [ms]
Bunny (Figure 7)	34,835	69,666	182.705	144.571	16.167	0.354
Hand, n=1 (Figure 8)	2,518	5,000	27.464	9.907	1.234	0.028
Hand, n=10 (Figure 8)	2,518	5,000	27.556	9.855	1.218	0.034

Table 2: Size of the scene and execution time of steps of the algorithm (in ms) for the hydraulic erosion simulations.

	vertices	faces	particles	iteration [ms]	calculate affected vertices [ms]	curvature calculation [ms]	laplacian calculation [ms]	vertex displacement [ms]
Bunny (Figure 10)	34,835	69,666	17,673	291.520	34.601	150.006	15.528	1.713
Canyon (Figure 11)	17,130	34,256	67,561	309.441	116.228	63.749	6.069	0.834
River undercut (Figure 15)	7,806	14,782	72,569	271.863	117.651	28.374	3.171	0.528
River flooding (Figure 16)	7,806	14,782	72,193	478.560	370.570	28.346	3.220	0.524

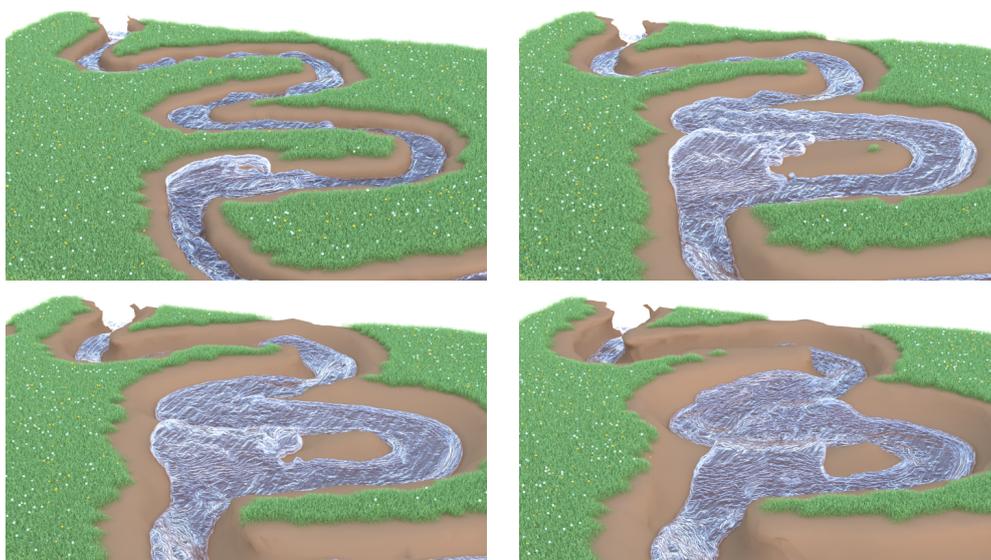


Figure 17: Fast water in the river erodes the river banks; front view. Top to bottom, left to right: original scene and the scene after 100, 200, and 300 iterations.

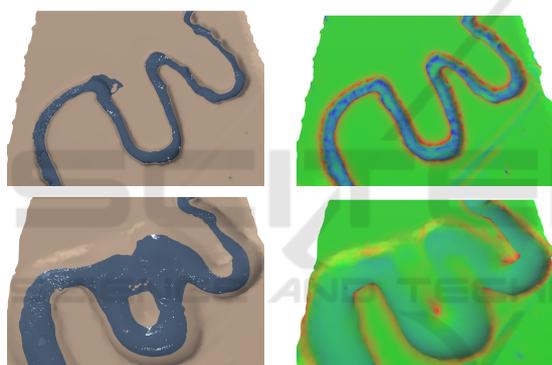


Figure 18: Simple rendering (left) and mean curvature values (right) for the simulation in Figure 16 for original scene (top) and the scene after 300 iterations (bottom). Using curvature color coding as described in Figure 2.

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