Accurate Real-time Complex Cutting in Finite Element Modeling

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Abstract:

This paper presents a real-time method for enacting accurate cutting of thin materials while retaining the physical accuracy of the underlying deformable material model. Our primary contribution is to offer a flexible real-time solution that can allow accurate cuts, re-cuts, curved cuts, sectioning (cutting out) on a deformable FEM model. Further contributions include improved handling of mesh element resizing after cutting for increasing material stability while balancing such resizing against real-time requirements. In this manner, we can represent precise cut incision (which may be curved or irregular) by subdividing mesh elements locally (at the cut point) while negating inappropriate (ill-shaped) elements with real-time level computational overhead and so avoiding modeling instabilities efficiently. We present the results of our solution that show the accuracy of the cutting method and illustrate timings for our optimised approach demonstrating its real-time qualities.

1 INTRODUCTION

As real-time simulations have provided models representing increased visual realism, matching this with physical interaction realism is required. One such interaction property that has received significant interest is that of cutting; acting cuts into simulated artifacts in real-time and having the results persist. It has been explored more in those applied areas of research that favor accuracy of precision and material behavior (e.g., simulated surgery) and less so in those favors aesthetics over interaction (e.g., video games). It brings about a balance between physical properties and aesthetic appearance in cutting. To achieve precision and accuracy while maintaining appropriate (believable) interaction requires a material model of advanced features that impact negatively on overall real-time performance.

The finite element method (FEM) is a common choice for constructing accurate models of deformable material behavior. The model has properties that allow accurate inspection of stress and other related parameters to determine the potential real-world behavior. FEM is computationally more expensive to achieve than its counterparts that afford visually pleasing simulations at the expense of physical accuracy (e.g., mass-spring). However, to achieve realism in cutting and leave a post-cut model that behaves as expected in the real world then FEM is a clear choice. However, difficulty arises in reorganiz-

ing the mesh of the FEM (the representation of the surface area) to ensure accurate cut depiction (the cut is where one desires) and resultant models still exhibit appropriate physical properties (no irregular behavior is introduced due to cuts). It requires a suitable algorithmic solution to ensure the reorganization, and possibly introduction or removal, of the elements (usually triangles) that constitute the mesh representing the model under dissection. Presenting algorithmic solutions that are engineered to work in real-time is the main focus of this paper.

Achieving accurate cut incisions does require elements to be altered or introduced. If a cut is to be presented exactly where a user needs, then elements must be reconstituted around this area, usually, it requires introduce additional mesh elements. However, achieving accurate cuts while making appropriately shaped elements is a non-trivial problem at the heart of a real-time FEM cutting technique. Ill-shaped elements relate to the inner working of the FEM; each element represents a unit of deformability that is solved to present an overall "shape" of the material model. As discretization is required as a step to attaining a practical solution, ill-shaped objects can inject significant errors in the cumulative mathematical calculations. It is compounded in real-time solutions where equation solvers accomplish a solution within a time boundary. A time boundary too low would provide insufficient time to achieve the desired mathematical accuracy that, ultimately, will cause the material model to fail.

The more complicated and flexible a material model is regarding cutting the more compounded the difficulty of ensuring real-time and physical accuracy. That is certainly true when allowing re-cutting as already altered and newly introduced mesh elements must be re-altered and managed while maintaining real-time behavioral properties. As mesh elements growing (more cuttings) so the computational expense increases and the possibility of ill-shaped elements also increases; this is when existing approaches tend to have the greatest difficulty, and many do not attempt re-cutting, especially in real-time scenarios.

In this paper, we continue the line of research into the cutting of material models using FEM. However, we present a general solution applicable to advanced material models that can be simulated in real-time. We present solutions to re-meshing of the material model after cutting that minimizes ill-shaped elements while accurately reflecting the exact position of the desired cut. Our novel approach provides convincing cuts that can be straight or curved, appear exactly where directed, allows re-cutting and the ability to cut-out (resulting in multiple FEMs) and do so while maintaining the physical properties of the cloth model itself.

2 BACKGROUND AND RELATED WORKS

Our primary focus is to generate aesthetically pleasing cuts to dynamic, responsive, material models while retaining accurate physics behavior in real-time. The cutting of deformable material has been an active area of research for many years (Wu et al., 2015). In this section we provide a broad discussion of techniques that use a variety of models, however, for brevity we only afford additional debate for those works that are focussed on (but not necessarily achieved together): (1) accurate cutting; (2) FEM; (3) real-time; (4) re-meshing.

2.1 Cutting

In mesh-based cutting techniques, non-progressive approaches have advantages by which computational overhead can be minimized using mesh subdivision determined as a whole, and present a cut at any desired point (Pietroni et al., 2009; Steinemann et al., 2006). An alternative approach is to use XFEM, where the cut can be described separately as a function on top of the higher order model (Kaufmann

et al., 2009). The latest work in this area is compelling, allowing cutting of 3D objects (Koschier et al., 2017). The placement of the cut can be very accurate. However, the cut edge can hardly inherit fundamental physics with the approximate enrichment basis functions.

Besides the persistence of cuts, the ability to re-cut areas must be considered carefully. As the topology of the mesh could be partially split numerous times before the current cut, care must be taken to assure the subdivision of the start and end elements is properly handled. The meshless model approach proposed by (Nesme et al., 2009) and polygon model (Sifakis et al., 2007) present abilities to re-cut, but such models are unlikely to find favor in real-time simulations that leave the underlying mesh altered.

2.2 Topology

Due to its relatively simple construction and convincing behavior the spring-based system (Baraff and Witkin, 1998) has been widely used for material modeling cutting (Cotin et al., 2000; Souza et al., 2014). Unfortunately, the model relies on the the springs connectivity and once the pattern is altered, behavior is not convincing. FEM employee dynamically reconstructs each of the element interactions based on the shape function, in this manner force is enacted across elements rather than independently across springs (Cakir et al., 2009). FEM then is exploited to provide more physically accurate deformations (Yeung et al., 2016).

Nonlinear FEM approaches employee nonlinear solver to handle deformation, while they are computationally more expensive than linear FEM. This can be largely mitigated with introducing co-rotational FEM (Georgii and Westermann, 2008). It adopts linear stress/strain solver on each element, and pre-compute a single stiffness matrix which is then simply transformed into the current configuration. It provides a fast FEM simulation with only a negligible overhead compared to mass-spring systems. Therefore it has been used in cutting simulations (Courtecuisse et al., 2010; Turkiyyah et al., 2011).

2.3 Subdivision

Subdivision algorithm provides an opportunity for recutting the same area on material models. Edge splitting changes the mesh connectivity (Souza et al., 2014; Yeung et al., 2016), whereas other methods such as vertex-snapping merely move the nodes to along cut path (Serby et al., 2001). Although it provides pleasing results, on a coarse mesh it can often

lead to jarring effects. For this reason, we handle edge splitting using current dynamic subdivision (Bielser et al., 2004) with the non-uniform subdivision. However, other edge splitting methods often result in formatting ill-shaped elements.

Adaptive subdivision schemes verify the level of subdivision depending on the force intensity acting on the mesh so that can produce a high-quality mesh in physics-based deformation (Bender and Deul, 2013; Narain et al., 2013; Koh et al., 2014), tearing (Pfaff et al., 2014) and force-based cutting (Seiler et al., 2011). These methods enforcing uniform subdivision avoiding ill-shaped elements. However, this also incurs a substantial computational overhead and thus in many cases a coarse subdivision level is defined.

The Delaunay approach has been used (Nienhuys and van der Stappen, 2004; Busaryev et al., 2013) to limiting ill-shaped elements. A further issue is the problem of computational complexity, although vastly optimized, Delaunay triangulation is still dependent on the problem size and can be computationally expensive.

3 THEORETICAL BACKGROUND

Mesh quality is a crucial factor in FEM-based cutting techniques for maintaining numerical stability and robustness of the simulation. The Delaunay refinement scheme is a well-established technique for maintaining mesh quality (Bowyer, 1981). It is achieved by ensuring that no nodes are created within the circumcircle of existing triangles, as illustrated in Figure 1. The effect of this is to ensure that the minimum angle of created triangles is maximized, thereby improving mesh quality.

The Bowyer-Watson algorithm reduces computation cost by eliminating the need for complex topological validity checks (Rebay, 1993). The approach incrementally inserts one node at a time, and then locally validates the triangulation of a subset of the desired points. It can take $O(N \times \log N)$ operations to triangulate N points. With the consideration of limited computation cost in real-time applications, we adopt the Bowyer-Watson algorithm to generate initial Delaunay triangulation.

4 IMPLEMENTATION

Our approach combines a Delaunay-based refinement technique (Bowyer-Watson algoritm) on co-rotational finite element modeling. It ensures that the higher computational cost of a subdivided mesh is focused on the areas of material closest to the simulated cut while maintaining the quality of the modified mesh. Furthermore, we apply a local split optimization process to handle the ill-shaped triangles.

4.1 Mesh Cutting

When operating subdivision method as the number of modification increases, there is a necessary trade-off of fidelity of simulation and mesh quality. Consequently, a technique which focuses on both the subdivision of elements in the area of the mesh most affected by the cut and the quality of generated mesh elements can lead to an optimal solution.

4.1.1 Locality of the Cut

The first step in simulating a cut to the material is to identify the triangles of the mesh that are affected. The process of Delaunay triangulation and incision generation will take place in the local coordinate space of the material mesh with no deformation due to external forces. However, the causes such as collisions takes place in world space, where the material is in a deformed state.

For our simulation, a mouse is used to identify the location of an incision in the world space. The position of the mouse in the 3D world space is translated to an un-deformed local space for the material mesh. The path of the incision is generated from a cubic Bezier curve which requires four control points (four mouse clicks).

Intersection detection will operate between the cut path and each edge of triangles of the mesh. Triangles with one or two line intersections will then be considered for generating initial Delaunay triangulation in the next stage of the algorithm. New points will be inserted at the exact place where the cut crosses the triangle edge.

4.1.2 Initial Delaunay Triangulation Generation

An example of traditional and Delaunay subdivision is shown in Figure 1. In the case of the traditional

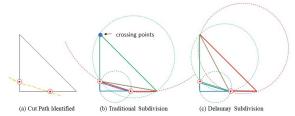


Figure 1: Delaunay generation principle.

subdivision, an ill-shaped triangle has been generated,

and there are nodes of other triangles within its circumcircle. The right diagram illustrates the Delaunay triangulation in which no circumcircle of any triangle in the triangulation includes nodes from other triangles.

The two instances of triangle cut types are illustrated in Figure 2. A new node is created on any in-

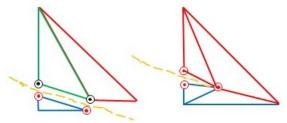


Figure 2: An example triangle with two intersection points (left), and an example triangle with one intersection point (right).

tersected edges at the position of intersection (i.e. one for each side of the cut at each intersection to open the cut incision. The Bowyer-Watson algorithm then regenerates the original triangle shape made up from constituent triangles with the three original points and new points. Consequently, the original triangle is subdivided into two or three constituent triangles. Especially, when a cut is terminate inside the triangle the original triangle will be replaced by four small triangles as shown on the right of figure 2, and the incision will also terminate inside the triangle. In the case of two intersection points, one of the triangles is separated by duplicated nodes.

Any ill-shaped triangles generated in this step will be recognized and grouped for the optimization operation

To generate arbitrary incisions (e.g. intersected cuts), the connectivity between the affected triangle and its neighbors is considered when opening cut incision. After recognizing an intersected edge, our method identifies whether there is another triangle that shares that edge. In that case, the new point and its duplicate are shared by the affected triangle and its neighbor.

4.1.3 Localized Optimization

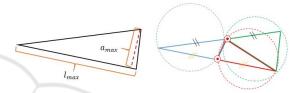
In the linear finite element method, the computational speed can be reduced by inefficient elements in the mesh. Consequently, optimal mesh generation and modification are required to produce high-quality mesh elements. This issue has been specifically identified in triangular meshes (Shewchuk, 2002) where irregular sizes or shapes of triangles can have a detrimental effect on computation time. While the Delaunay algorithm can maximize the minimum angle of

all triangles in the triangulation, this does not guarantee that no ill-shaped triangles will be generated. To address this problem, we introduce local split optimization to increase the quality of the modified mesh.

We identify the aspect ratio as the parameter to efficiently evaluate our generated triangles. For triangular meshes, aspect ratio is defined as:

$$AR = l_{max}/a_{max} \tag{1}$$

where l_{max} is the length of the maximal edge, and a_{max} is the height measured from this edge. The approximate minimum possible aspect ratio for the original triangles in the mesh is 2. In our local split optimization algorithm, newly generated triangles whose aspect ratio is more than 3 will be re-triangulated as shown in the right of Figure 3. The steps of our opti-



(a) A ill-shaped triangle: $l_{max}/a_{max} > 3$ (b) Local Split Optimization Figure 3: An example of the localized optimization.

mization operation are:

- The two longest edges are selected first;
- New points are inserted at the mid-point of the selected edges;
- Any ill-shaped triangle (as defined by aspect ratio) is regenerated by the Delaunay algorithm;

The introduction of new points necessitates the subdivision of the triangles that are directly adjacent to the new points (referred to as the 1-ring triangles). During the subdivision step, if an edge is subdivided, but its neighbor is not, a discontinuity can be created (as illustrated by the shaded section in Figure 4) in the form of a crack. Avoiding this cracking of the mesh, the neighboring 1-ring triangle is also subdivided with the new points, replacing the triangle with two constituent triangles (as shown in the right of the figure). Note that only one of the 1-ring triangles requires this subdivision (rather than all of them as in the more generalized subdivision methods). Furthermore, if there is any ill-shaped triangle created during this step, our optimization process will keep operating until the triangulation is under the acceptable level.

4.2 Topological Modification

Employing a linear elasticity model with an implicit integration scheme allows us to generate a fast and



Figure 4: A crack appears when its neighboring triangle has been subdivided (a), 1-ring neighbors of subdivided triangles are split as well (b).

stable simulation. However the approach can also result in unrealistic or unstable effects when large deformations are needed. To resolve this issue, we use corotated finite element modeling (Felippa and Haugen, 2005; Georgii and Westermann, 2008), which extract the non-linear part of the current deformation before computing the forces.

As cutting of a mesh necessitates disconnecting parts of that mesh, a topological modification is required. Changing any element of the global matrices invalidates any previous factorization, necessitating a refactorization of the matrices. Rather than reconstructing the global matrix in each time step, we incrementally update the global matrix from the current state in two steps: index replacement and element addition.

4.2.1 Index Replacement

In contrast to current methods, we change the vertex indices of all intersecting faces so that the contributions of the original elements are not removed but replaced in the global stiffness matrix K. For instance, if in time (i) the cut path passes through the element S_e two vertex indices of the element are replaced by the indices of new points to fill in one side of the incision. In the next step (i+1) the element stiffness matrix K_e must be updated. The initial area A_e will be calculated from the new vertex positions. As discrepancies in vertex indices can lead to computational inefficiency, we mitigate this effect by changing the vertex indices in this step.

4.2.2 Element Addition

After the index replacement step, new vertices are created to prepare for element modifications, so the dimension of matrices will be increased to accommodate the new vertices. Rather than reconstructing the global matrix in each time step, we incrementally update the global matrices. For instance, the stiffness matrix K is updated to:

$$K' = K_0 + \sum_{i=1}^{m} G_i K_I G_i^T$$
 (2)

where K_0 and K' represent the current stiffness matrix in this time step i and the updated stiffness matrix in next time step i+1, m is the number of new elements, K_i , G_i and G_i^T are the matrices which map the rows and the columns of the new element metrics to the global matrix. The mass and damping matrices must also be updated in an equivalent way.

The new vertices introduced in the subdivision of the cut triangle, and the affected neighboring triangles, are each added to the global matrices in this manner. This dynamic approach, incorporating each new vertex into the index list incrementally (in two steps as described), is more computationally efficient than recalculating the global matrix for the entire mesh.

4.3 Time Integration

We employ an implicit time-based solver to simulate the evolution of the visco-elastic deformable surface model.

$$M\frac{d^2x}{dt^2} = Kx + \overline{K}\overline{x} + \widetilde{K}x + f_{(v)} + f_{ext}$$
 (3)

Where x is a matrix containing each of the n vertices in the model. For the time step t when the cutting path is instigated, computation is completed by the following steps:

- Compute the rotations R_e for each triangle.
- Update the stiffness matrix K with the two steps described in section 4.2, assemble the global matrix \widetilde{K} (rotate the result of multiplication back to 3D space), and compute the viscous bend force $f_{(v)}$ with velocity v.
- Compute $\overline{K}\overline{x}$, where \overline{K} and \overline{x} stand for the stiffness matrix and the vector of position in the rest state respectively.
- Calculate the total forces f_{ext} which include gravity and any other external force.
- Carry out an implicit time step.

The key of this procedure is that the system of equations to be solved in each time step is linear. The linear system is been solved by a conjugate gradient method. Our topological modification method decreases the computation involved in recomputing the matrix for every node, as we incrementally add nodes through re-indexing.

5 RESULTS AND DISCUSSION

In this section, we discuss the performance of our approach in a variety of contexts, including visual

outputs for complex cuts, computation time, mesh quality and level of detail of cut surface. The algorithm was tested on a series of meshes ranging from 800 triangles to 12800 triangles, and for each resolution the simulation operation was repeated 10 times to obtain the average computation time. All experiments were run on a desktop PC, equipped with an $Intel^{\textcircled{R}}$ $Core^{TM}i7-4790S$ CPU @ 3.20GHz processor (we use a single core), 16GB of RAM, and NVIDIA GeForce GTX 980 graphics card. Dynamic simulations of the proposed implementation can be found in the accompanying video linked to https://youtu.be/Yug16Wi1GgA.

5.1 Complex Cut Surfaces

Our method can produce realistic and accurate cut surfaces with arbitrary shapes even in low-resolution meshes. Note that all meshes illustrated in figures are constructed by 800 initial triangles. Figure 5 shows two example cuts (straight and curved). Figure 6 illustrates partial cuts which include cut from an edge (the left) and cut part of mesh entirely out (the right). Figure 7 shows a re-cut (the left) and multiple cuts (the right). Within a single mesh. Intuitively, our method can provide a high-detailed cut surface independent of resolution requirements. Moreover, the visual outputs also demonstrate how our method can produce realistic cut incision with accurate physical behaviors which involve substantial bending, swirling and flipping.

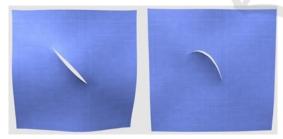


Figure 5: Different shapes of single cut within a mesh. The left shows a straight cut, while the right shows a curved cut. Both simulations use a mesh of 800 initial triangles.

5.2 Mesh Quality Comparison

We present a localized optimization to efficiently remesh the ill-shape triangles and their one-ring neighbors. Figure 8 compares the mesh after our cutting simulation with the method that simply subdivides intersected triangles with a static re-connect order (conventional subdivision). Intuitively, the conventional subdivision can easily generate ill-shaped triangles



Figure 6: Examples of cuts that (left) cut from a side and (right) cut part of the mesh out. Note that each subdivided mesh subsequently has an independent deformation basis function.



Figure 7: High-detail cut surfaces which demonstrate intersected cut (left) and multiple cuts within a single mesh (right).

leading to unexpected cut edge distortion and abnormal deformation. In contrast, our method can avoid ill-shaped triangles, making the simulation numerically stable and visually convincing. Furthermore, we locally increase the details only around the incision; therefore the rest of the mesh maintains the level of detail to ensure a focused computation cost.

Figure 9 illustrates how our adaptive subdivision scheme generates optimal triangulation with low average aspect ratio (less than 3). We implemented the conventional subdivision which simply subdividing original triangle into three along the cut path on the same size model. As shown in the figure, the conventional subdivision can easily generate inefficient shaped or sized triangles with a high aspect ratio. In contrast, our method optimizes all such triangles whose aspect ratio is more than 3 to re-generate a stable and physically accurate incision.

5.3 Computation Cost Measurement

Table 1 shows the average computation times per simulation step for various levels of mesh resolution. We apply an implicit time-based solver for the viscoelastic deformation. The first column represents the scale of mesh, which followed by geometry modification cost that relates to the initial Delaunay triangulation generation and localized optimization. The third column is the physics updating time after the re-meshing

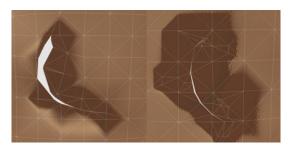


Figure 8: With simply subdividing intersected elements without further optimization (left), it leads to a swirling cut edge. In contrast, our method (right) provides smooth, physically accurate incisions.

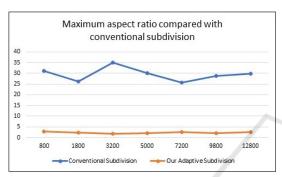


Figure 9: Comparison of maximum aspect ratio after cutting operation with conventional subdivision that without any further optimization.

operation is completed. The last column shows the total computation time of each cutting experiment.

The results indicate that our algorithm provides a fast cutting process. Even in the highest quality model (12800 triangles), the total computation time in each call of our cutting method is less than six milliseconds. Moreover, the differential value of the total time taken between the 800 triangles mesh and the 12800 triangles mesh is only 3.915 milliseconds, which suggests that our cutting method can be integrated into a high-quality model simulation in real-time.

Table 1: Performance measure (ms).

Triangles	Geometry	Solver	Total Time
800	0.865	0.203	1.068
1800	0.947	0.278	1.225
3200	1.246	0.356	1.602
5000	1.987	0.390	2.377
7200	2.935	0.683	3.618
9800	3.598	0.702	4.30
12800	4.130	0.853	4.983

5.4 Level of Details Comparison

Figure 10 compares the level of details around the cut incision with conventional subdivision (which only subdivide the intersected triangles into three smaller triangles along the cut path). Our method optimizes the triangles generated by subdivision, with a small number of additional DOFs.

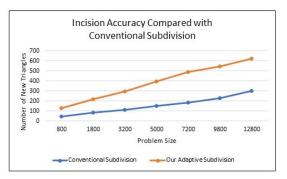


Figure 10: Comparison of the level of detail around the incision with conventional subdivision scheme without further subdivision.

6 CONCLUSION AND FUTURE WORK

The cutting method described in this paper introduces three novel contributions to the area of 3D simulations of mesh cutting using FEMs. The first significant contribution is the method of adopting the most efficient incremental Delaunay generation algorithm, Bowyer-Watson algorithm, performing lower computational overhead than existing algorithms to generate appropriate triangulation with low aspect ratio after cutting occurs. Secondly, we achieved robust simulation of complex cuts, such as re-cuts and intersected cuts. Finally, we generate the optimal modified triangulation by operating the local split optimization to efficiently handle ill-shaped elements maintaining the mesh quality with the maximum aspect ratio in the triangulation of less than 3.

Our future work will focus on fusing the surface model topology with the geometric model to produce a component-based model to simulate detailed skin model.

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