Musculoskeletal System Modelling Interpolation Method for Muscle Deformation

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Abstract: In this paper we present an interpolation method that was derived from the muscle deformation algorithm computed on the gradient domain deformation technique. The method uses linear constraints to preserve the local shape of the muscle and the non-linear volume constraints to preserve the volume of the mesh. The Gauss-Newton method with Lagrange multipliers is used as the main computation algorithm and the interpolation approach serves especially to smooth up deformation steps. Thanks to the interpolation of main bones movement positions by several temporally interpositions, the large distances are optimized and the muscles of the musculoskeletal model are deformed in a more realistic way. The method was implemented in C++ language, using VTK framework and was integrated into the human body framework. Despite the fact that the current implementation is not optimised, all muscles tested were processed in a few minutes on commodity hardware, which is much faster in comparison with the traditional FEM approaches.

1 INTRODUCTION

The musculoskeletal modelling and simulation is an important step in predicting and personalizing the treatment for the osteoporosis patients. In the VPHOP project (VPHOP, 2012), we aim, therefore, at creating a virtual multi-scale model of human body that could be used for the simulation of the fracture in dependence on the measured parameters and patient physical predisposition.

Starting from an atlas model of a cadaver, we perform patient-specific adjustments to get a model that conforms to the patient's anatomy. This model is then fused with the motion data of the movement to be investigated. The positions and shapes of the muscles during motion must be calculated, interpenetrations being avoided so that muscles wrap properly around the bones and other muscles. All calculations must be performed quickly so that the approach is useful for clinical practice. This is a challenge that will be address in this paper.

For testing purposes we use data for pelvis and especially right leg. Our data consists of bones and musculo-tendon units (aka muscles) represented by triangular surface meshes, attachment areas of muscles (sites where muscles are attached by tendons to the bones) and of action lines, straight or piecewise straight lines joining the points at either end of the muscle where it is attached to the skeletal bones, since our approach comes out from the action line models used in biomechanical practices, e.g., (Any-Body, 2010), (OpenSim, 2010). An action-line in our data is a poly-line passing through one or more via points, which, although being a popular choice, negatively influences the quality of results. We note, however, that one could compute a skeleton from the mesh of the muscle and use it as a more accurate action line to increase the reliability of the approach.

The remainder of this paper is structured as follows. In the next section, we give a brief survey of existing methods, the basic deformation method is outlined in Section 3, and the proposed interpolated version of this deformation method is described in Section 4. Results are discussed in Section 5. Section 6 concludes the paper.

2 RELATED WORK

In biomechanics, muscles are traditionally represented by action lines because, although this does not provide essential features of the muscle dynamics, using much more accurate representations based typically on FEM meshes, e.g., (Blemker et al., 2005), is highly impractical in the clinical context due to their large time requirements (several hours

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on a supercomputer). Our approach, which is inspired with the techniques of computer graphics, attempts at bringing a compromise by representing a muscle with a surface mesh that quickly deforms.

Most popular computer graphics methods for deformation of the surface mesh are based on meshskinning technique, e.g., in (Blanco et al., 2008), that binds a mesh to the underlying skeleton so that change of this skeleton produce a smooth non-rigid deformation of the mesh. However, these methods often fail to preserve the volume of the object being deformed, e.g., (Ju et al., 2005), and they do not induce impenetrability between objects, which is undesirable for our purpose.

Shi et al. (Shi et al., 2007) proposed an approach in which, for each vertex of the mesh, an equation describing the energy of this vertex derived from its position is formed and the approach tries to successively reposition vertices to minimize the total energy. Each time the intersection between two meshes is detected, a new equation describing the impulse force at the intersected area is added into the system.

Our approach is similar to the one by Shi et al. The most significant differences are as follows. To speed up the process, we do not minimize the energy of the original mesh but of a coarse mesh and then transfer the computed values to the original mesh. We solve the intersections locally because this gives us a better control than the impulse force approach.

3 DEFORMATION METHOD

Bones, action lines, and muscles are positioned in the rest pose (RP), which is the initial position for the deformation algorithm. For bones and action lines also their final position, called current pose (CP), is available. To get a muscle from RP into CP, the deformation of the muscle has to be provided. An example can be seen in Figure 1.



Figure 1: Position of bones (pelvis and femur) and shape of the gluteus maximus: a) muscle and bones in RP; b) bones in CP, muscle in RP; c) muscle deformed to CP.

The original method is based on algorithm described in (Huang et al., 2006). For each muscle, its outer hull (a low polygon coarse mesh) is needed. Mostly it is loaded from the pre-computed database; if not available, the hull is computed by the progressive hull decimation algorithm (Cholt, 2012). This coarse hull is used to get an initial approximate solution, which is then refined by a final few iterations in which the original mesh is used. This strategy saves both memory and computational power.

The deformation algorithm as described in (Kellnhofer et al., 2012) defines constraints to preserve the shape of the muscle, its main deformation direction and its volume. From these constraints the over-constrained linear system with non-linear boundary constraint of volume was mathematically derived. We solve the equations iteratively using Gauss-Newton method with Lagrange coefficients. In each iterative step, a new position for every vertex of the mesh being processed (either the coarse hull mesh or the full mesh) is computed, after which the intersection corrections are applied to avoid mutual inter-penetration of meshes.

3.1 Solving Intersections

During the whole deformation, computation intersections are solved on two levels. In each iterative step, it is checked, if the deformation has not moved the mesh vertices too far. Because it profits from the knowledge of the previous vertex position and its motion, it is called dynamic intersection. As can be seen in Figure 2, if any vertex is found to lie inside an obstacle, the adequate triangle of the obstacle in the direction inverse to the vertex motion direction is detected and the vertex is moved to the boundary of the obstacle (on the detected triangle) – left gray point in Figure 2; or to its previous position, if the vertex has been already inside the obstacle before the deformation step – right gray point in Figure 2.



Figure 2: Dynamic intersection solving schema (colour curve represents the obstacle, black curve the deforming muscle): a) the original position of vertices (solid line) and the intersected vertices after deformation iteration (dashed line); b) situation after intersection solving.

As each vertex of the original muscle mesh is defined as the linear combination of all vertices of the hull, the linear mapping is not able to represent a larger pit pushed into the original mesh surface and, therefore, after all iterations, the final intersection check, called static intersection, using full meshes must be done to prevent problems. Because we need to check the relative position of muscles and obstacles, we cannot use any information about the previous movement; the detection starts from the relative positions of computed meshes. Intersected vertices are grouped, for each group its central point is computed (as an average position of all group vertices) and all vertices of the group are moved to the nearest triangle of the intersected object. An example can be seen in Figure 3.



Figure 3: Static intersection solving schema: a) central point position and direction of vertices movement (red dotted lines); b) intersected vertices moved to the correct position on the border of the obstacle surface.

4 INTERPOLATION METHOD

The original deformation method described above works well and quite quickly. But when we have a look on its result in detail (e.g. in Figure 4) the sharp cut of the bone into the muscle surface computed by the original method can be seen well (in this example pelvis bone and the gluteus maximus were used). The enlarged detail can be also found in Figure 12a.



Figure 4: Result of the original deformation method.

This result is caused by static intersection being solved just once. It would be advantageous to run the static intersection solving several times to keep the print of bones in muscles smooth and to deform muscles more realistically.

Another problem emerges, if we have two muscles touching a bone in RP, as it is outlined in Figure 5(a). After moving the bone into CP, the bone intersects one of these muscles completely (b). As the dynamic intersections are being solved in each iteration step, the muscle vertices, which are intersected before the deformation, remain intersected. The result can be seen in Figure 6: the shape of the muscle is incorrect as the muscle is fixed on the bone.

The basic idea of the proposed modification is simple: if the distance between RP and CP positions is too large, we create several artificial inter-steps in between because the static intersection will then move the muscle mesh vertices for a smaller distance and one can expect that sharp unrealisticlooking pits would be avoided. To create these intersteps, we have to interpolate all obstacles and also action lines. Both interpolations are described in the following sections.



Figure 5: Schema of position of muscles and bone: a) all in RP without any intersections; b) muscles before the deformation in RP, bone already in CP.



Figure 6: Rectus femoris computed by the original deformation method.

4.1 **Bones Interpolation**

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As bones are represented by triangular meshes, their vertices can be interpolated separately as:

$$x_i = rp_i + j^*(cp_i - rp_i)/stepCount$$
(1)

where x_i are coordinates of the i-th vertex in the j-th interpolation, rp_i is the i-th vertex of the RP mesh, cp_i represents coordinates of the same vertex in the CP, *stepCount* determines the number of interpolation steps. In Figure 7, all interpolation positions of the right leg can be seen.



Figure 7: Pelvis, right thigh and shank bones in interpolated positions.

4.2 Action Lines Interpolation

As the poly-lines representing the RP and the CP paths of the action line may not have the same number of points, or the distribution of points along these poly-lines may be very different, first we must ensure that both poly-lines are matched (both have the same number and distribution of points) to simply interpolate them.

Let us assume that the RP poly-line C is formed by the points $P_0 \dots P_m$ and the CP poly-line C' by the points $P_0' \dots P_n'$. The matching starts with an arc-length parameterization of both poly-lines, i.e., to points P_i and P_i' , we assign the parameters t_i and t_i' , respectively, such that:

$$t_{i} = \frac{\sum_{k=1}^{i} |P_{k} - P_{k-1}|}{\sum_{k=1}^{m} |P_{k} - P_{k-1}|}, t_{i}' = \frac{\sum_{k=1}^{i} |P'_{k} - P'_{k-1}|}{\sum_{k=1}^{n} |P'_{k} - P'_{k-1}|}$$
(2)

Hence $t_0 = t'_0 = 0$ and $t_m = t'_n = 1$. The points of the RP poly-line are now processed. Given the point P_i , the algorithm searches, in increasing values of j, for a point P_i' that has not been already matched and for which $|t_i - t_j'|$ is smaller than some allowed tolerance ε . If the outcome of the search is negative, a new point P_i is introduced on the CP poly-line at the location for which the parameter value $t_i' = t_i$. The points P_i and P_i' are then said to be matched. Any as-yet-unmatched points on the CP poly-line are then processed using a similar approach. By the end of this process, both poly-lines will have the same number of points and these points will be matched. The overall matching process is shown in Figure 8.



Figure 8: Matching the RP poly-line P₀, P₁, P₂ and the CP poly-line P₀', P₁', P₂', P₃' - arc-length parameterization of both poly-lines.

When RP and CP action lines are matched, the interpolation can be done in the same manner as in the case of bones. In Figure 9a, the original action lines and their points can be seen (action line in RP is represented by the green curve with blue points, the action line in CP is figured as blue curve with green points). Figure 9b shows the matched RP action line and the interpolated first step action line. The triangle mesh around the action lines is the hull of deformed muscle hull in RP.

4.3 **Deformation Computation**

Let us assume three-step interpolation (the number of steps can be specified either by the user or com-

puted automatically from the largest distance difference between the vertices of the original RP and CP), i.e., we have four positions: $RP = P_0$ (see Figure 10a), P_1 , P_2 and $P_3 = CP$. The method starts with the calculation of paths of action lines and positions of vertices of bones at P1 and P2 using linear interpolation of those at P₀ and P₃. Afterwards, the original deformation method is run to wrap muscles from P_0 into P_1 (Figure 10b), after which it is run again to wrap muscles from P_1 to P_2 (Figure 10c) and finally, in a successive run, to wrap these muscles into the final position P₃ (Figure 10d).



Figure 9: Action lines of illiacus; RP (the more curved one) is surrounded by the triangle surface of muscle hull: a) the original action lines (green curve with blue points in RP, blue curve with green points in CP); b) recomputed action lines for the first step of the interpolation.



Figure 10: Steps of the interpolation process: a) RP of the muscle and first interpolated position of bones and action lines (P₀); b, c) starting position of second and third interpolation steps (P_1 and P_2); d) final deformation state of the muscle (P₃).

5 RESULTS

Figure 11 shows the impact of the proposed new method on the static intersection in the case of gluteus maximus and pelvis. The original method (a) shifts the vertices for approx. double distances than the interpolation method (b) and majority of them are shifted for a similar distance, while in the new method the shifting distance decreases to the borders of the intersected area. This means that the created bone print shape is smoother. Moreover, each following interpolation step deforms the semi-result and so any sharp edge is smoothed.



Figure 11: Static intersection solving (line segments represent the trajectory of moved vertices): a) at the end of the original method computation; b) during the last interpolation step.

Figure 12 compares the shapes of muscles deformed by both methods. It can be seen that the muscle provided by the new method does not contain any sharp edges of the pit and the gradual borders of the pit seems to correspond more with the real forming of a consistent muscle.



Figure 12: Result of contact area of gluteus maximus and pelvis computed by: a) the original method; b) the interpolated deformation method.

The only problem, which has yet to be resolved, is the high computational time. Its main reason is that it is necessary to construct a new hull before each step because the static intersection solving at the end of the interpolation step modifies the original mesh and while it is possible to easily get the original mesh from the hull (thanks to the linear mapping of vertices) it is not possible so far to provide the reverse process. The computation of muscle deformation needs just several seconds to get results, as mentioned already in (Kellnhofer et al., 2012). If we provide it several times to get the interpolation semiresults, the computation needs still seconds to finish, but before each interpolation step the outer low polygon hull has to be computed again.

The progressive hulls decimation algorithm needs easily a minute on commodity hardware to compute a new hull and if we need to repeat it several times during the whole interpolation, the computational time grows with each single step. Because it is not possible to provide the whole computation on a hull or to avoid the static intersections, our future research will be focused on possible approaches on reverse (full mesh to hull) computation.

So far one single muscle deformation together with surrounding bones was described. The human body contains of course many muscles which are placed close to each other and so if more muscles are taken into the deformation method, it should keep the bilateral influence. Figure 14a shows the difference between the single muscle deformation. The muscle together with involved bones can be seen also in Figure 13. Parallel deformation of gluteus maximus and gluteus medius is shown in Figure 14b-c. (in Figure 14c, only gluteus maximus is visualized and so impact of gluteus medius is visible in the bottom part of the visualized muscle).



Figure 13: Gluteus maximus computation; computed bones (pelvis and femur) are visualized.

There was one more problem described in Section 4: fixing of the muscle on the bone because of the dynamic intersections. The result of interpolation method for the used example – rectus femoris can be seen in Figure 15. Thanks to the smaller movements of the bone, no problems appeared.



Figure 14: Results of the interpolated deformation method (4 steps of interpolation were used): a) gluteus maximus computed only with bones (no other muscle); b) gluteus maximus computed together with gluteus medius; c) visualization of result from (b), gluteus medius is hiden.



Figure 15: Rectus femoris computed by the interpolated deformation method.

6 CONCLUSIONS

We have developed method for deformation of muscles in the musculoskeletal model of human body. Despite of its high computational time (though it is still much lower than in case of FEM methods), the interpolation method seems to be an interesting supplement to the currently used one-pass deformation method especially in such parts of the model, where the difference between the initial and final position of bones is too large to provide the computation at once and where the large bones are pressed into muscles. Moreover, the further research and optimization of original mesh to muscle hull conversion may help to decrease the computational time so that the well looking results could be used also in the real time model processing.

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