

SPECTRUM WEIGHTED HRTF BASED SOUND LOCALIZATION

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Abstract: In the framework of humanoid robotics it's of great importance studying and developing computational techniques that enrich robot perception and its interaction with the surrounding environment. The most important cues for the estimation of sound source azimuth are interaural phase differences (IPD), interaural time differences (ITD) and interaural level differences (ILD) between the binaural signals. In this paper we present a method for the recognition of the direction of a sound located on the azimuthal plane (i.e. the plane containing the interaural axis). The proposed method is based on a spectrum weighted comparison between ILD's and IPD's extracted from microphones located at the ears and a set of stored cues; these cues were previously measured and stored in a database in the form of a Data Lookup Table. While the direct lookup in the table of the stored cues suffers from the presence of both ambient noise and reverberation, as usual in real environments, the proposed method, exploiting the overall shape of the actual frequency spectrum of the signal, both its phase and modulus, reduces dramatically errors in the localization. In the paper we give also the experimental evidence that such method improves greatly the usual HRTF based identification methods.

1 INTRODUCTION

In humanoid robotics applications main sensory apparatus are vision and hearing. While vision undoubtedly provides main spatial details of surrounding environment, it is the sense of hearing that enriches perception of new and invaluable information: it gives, for example, precious information due to sudden changes in the scene. In few words it is for communications purposes that the ability to produce and localize sounds becomes mandatory.

The term CASA (Computational Auditory Scene Analysis) denotes the group of techniques that try to mimic the behaviour of human auditory system, or at least some of its features which appear to be more relevant for the identification of sound sources. Binaural Localization denotes the task of estimating sound source position based on the analysis of signals collected at the ears; the role played by the head is essentially that of filtering incoming sounds in order to feed all necessary information to the brain so that both azimuth and height localization of sound source posi-

tion may take place.

The modifications on the incoming signal as collected at the ears can be successfully modeled by a linear filter whose transfer function is called Head Related Transfer Function (HRTF); binaural information (cues), mainly phase and intensity differences, can be obtained from a measured set of HRTFs, yielding azimuth data lookup models (Algazi, D'uda, Thompson and Avendano 2001).

1.1 Earlier Works

In the last years several computational methods have been developed for the extraction of sound source azimuth angles from binaural signals.

Some of them are based on the coincidence model proposed by Jeffress in 1948 (see (Joris, Smith and Yin, 1998)). This is a model of the neural system where nerve impulses from each of the two ears propagate along delay lines in opposite directions. At the position where the impulse coincide a nerve cell is excited, effectively transforming time information into

spatial information. A method to evaluate this ITD delay over time is that of computing a running short-time cross correlation between signals collected at the ears (Knapp and Carter (1976)). In this method, if signals are previously filtered, we can successfully take into account the actual spectrum of the incoming signal in order to reduce at some extent the effect of noise and reverberation. However the failure rate of the identification methods based on the Generalized Cross Correlation, when used at practical values of SNR results relatively high, thus preventing in many cases real time applications.

Another method, proposed in (Viste, 2004) and (Evangelista and Viste, 2004) is based on joint evaluation of the ITD and ILD cues obtained by means of a running Short Time Fourier Transform (STFT); here the ILDs are used in order to resolve the ITD ambiguity due, as is well known, to phase ambiguity: in this method, gross identification is performed by means of ILD, while ITD evaluation is used to improve azimuth estimate. This method, since it performs the evaluation at each frequency bin, is suitable to take into account bin per bin weights as in our proposal.

A third class consists in methods based on a very strict sensory fusion as in Hokuno (see (Nakadai, Okuno and Kitano 2001)). These also may take advantage of an improved calculation based on acoustical cues, as in our proposal.

The last class to be taken into account is based on the use of a neural network trained with cues extracted from binaural signals as discussed e.g. in (Irie (1995)); even in this case the proposed method of weighting cues may be invaluable.

Our proposed implementation may thus be embodied in existent architectures, improving their performance and robustness.

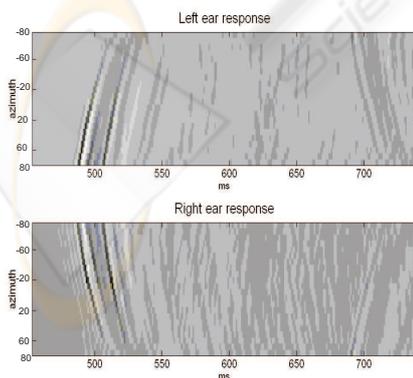


Figure 1: HRIR measured for both left and right sides.

1.2 Contribution

The method here exposed belongs to the second class of methods summarized in the previous section; his starting point is (as in (Viste, 2004) and (Evangelista and Viste, 2004)) the measure of the set of HRTFs on a grid of positions corresponding to several different azimuth angles (in fig.1 we show their time domain counterpart: the Head Related Impulse Response HRIR); from these transfer functions we obtain the $ILD_h(\theta, \omega)$ and the $IPD_h(\theta, \omega)$, functions of azimuth θ and frequency ω , evaluated at discrete angular positions and frequencies.

The $IPD_m(\omega_k)$ and $ILD_m(\omega_k)$ measured¹ time by time from an observed signal pair at the robot ears using Short Time Fourier Transform (STFT), are compared against the HRTF data set in order to obtain an estimate of the source azimuth: the position yielding minimum deviation from the stored table is selected as true azimuth. This is referred to as HRTF Data Lookup: azimuth estimates by use of this techniques are based on ILD and IPD separately.

In our proposal estimate of the angle is obtained by minimizing the error, properly weighted in frequency (as shown in section 3), made by comparing these cues with the $ILD_h(\theta, \omega)$ and $IPD_h(\theta, \omega)$ functions stored in the Data Lookup Table; the effect of weighting is clearly seen in fig.2 where the straight deviation from a curve in the table at a specific azimuth is shown in the upper part of the figure. In the lower part the same deviation is weighted by an evaluation of the signal spectrum: only the bins in the spectrum where signals is larger and than exhibit higher SNR are taken into account.

The signal used in the figure shows narrowband contents limited to a small part of the frequency axis.

The comparison is made all over the frequency axis or, more successfully, in selected frequency bands; in fact on the ground of Duplex Theory ((Blauert (1997))) the ITD and ILD cues are significant in different and complementary frequency ranges, mainly low range for ITD and high range for ILD.

The position in the azimuth grid corresponding to a minimum in the weighted error function is chosen as the best estimate of sound source position,(see figure 3, where the successful estimate in weighted case is -24, while unweighted method shows a clear error, estimating -6 as azimuth sound position). Also, based on the evaluation on the whole grid, a measure of the reliability of the measurement may be given in form of error ratio between neighbor azimuth positions.

¹The subscript h refers to the HRTF cue while subscript m refers to the measured cue

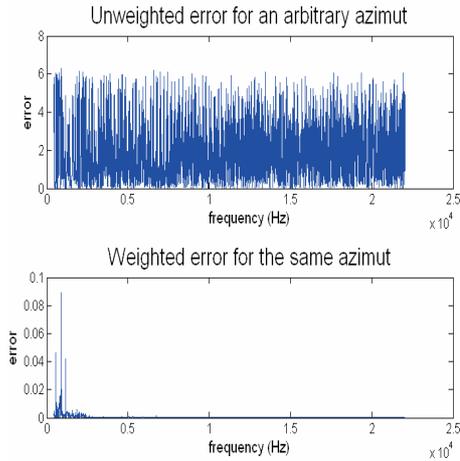


Figure 2: Unweighted and weighted error as function of the frequency for an arbitrary azimuth.

It is seen from the figure that the weighting method, grants higher error margins and therefore exhibits greater reliability and robustness.

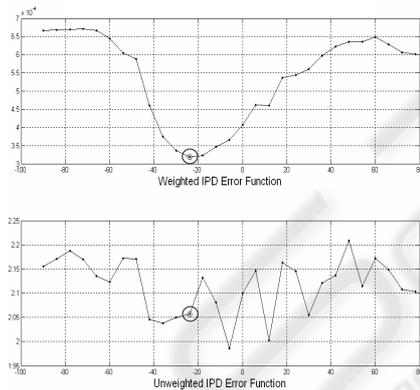


Figure 3: Weighting the Error Function clearly sharpens its minimum peak.

2 CUE ESTIMATION

2.1 ILD

The ILD cue is mostly due to sound shadowing by the head, an effect which is highly frequency dependent; outer structure of the ears (*pinnae*) also affect this dependence. At low frequencies where wavelength is comparable to the size of the head, shadowing may be neglected, while at higher frequencies it becomes more consistent, delivering level differences up to tens dB. Theoretical formula for this de-

pendence is very complex (see (Nakadai, Matsuura, Okuno and Kitano, 2003) for a version of it) while it's not hard to extract it from the binaural signals: if p_r and p_l are the sound pressures at the ears, ILD in dB is given by:

$$ILD = L_p^{(r)} - L_p^{(l)} = 10 (\log_{10} p_r^2 - \log_{10} p_l^2) \quad (1)$$

where the signal spectra are evaluated by means of DFT, expression of the ILD for each frequency bin simply becomes the ratio in dB of the different bin amplitudes of right to left signals:

$$ILD[k] = 20 \log_{10} \left| \frac{Y_r[k]}{Y_l[k]} \right|$$

2.2 ITD, IPD and Unwrap Problems

The difference in the path that a sound wave covers to reach the two ears results in a time and phase difference between the waveforms collected at the ears. If we consider a spherical head with radius $r = \frac{d}{2}$, where d is interaural distance, neglecting the shadowing effect of the head and under the hypothesis that the distance R of the sound source is much greater than d , time difference is given by :

$$\Delta T = \frac{\Delta \rho}{c} \simeq \frac{2r \sin \theta}{c} \quad (2)$$

where $\Delta \rho$ is the difference of path between the two incoming waves and c is the speed of sound. If $X_r[k]$ and $X_l[k]$ are the binaural signal spectra, the resulting estimate of ITD for each bin is:

$$ITD[k] = \frac{-IPD[k] \cdot L}{2\pi \cdot k} \quad (3)$$

where IPD is given by

$$IPD[k] = \arg \frac{X_r[k]}{X_l[k]} \quad (4)$$

Here the usual problem of proper unwrapping, i.e. correct choice of the $2\pi n$ offset to be added at wrapping points, is met: this offset in fact depends on both frequency and sound source angular position and cannot be defined *a priori*; this problem furthermore is increased by uncorrelated noise between the two signals.

We overcome this problem avoiding the calculation of ITD and simply using the rough wrapped IPD cues. Actually in this way the comparison is made between the general shape of the phase (and its derivative) for each segment where this function may be

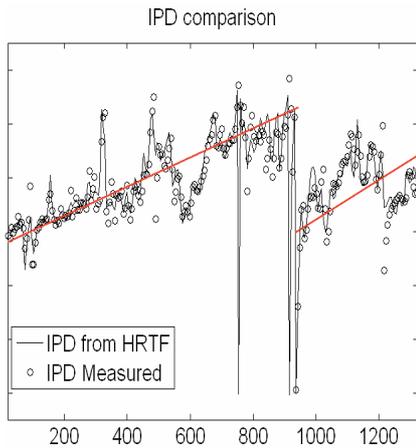


Figure 4: Close lookup of IPD function for both HRTF and measured cues.

considered as continuous in frequency; this is clearly shown in fig.4 where we show a close look-up of the straight phase difference from the true azimuth in the reference table and, superimposed, the same difference from the measured signals: their apparent similarity, resulting in low values of the difference between the measured values and their stored counterpart is the basis of this table lookup method.

In fig. 5 we show the histogram of the derivative of the phase function computed as the difference from sample to sample; out of range values, due to discontinuity at wrapping frequencies are easily discarded by means of a simple statistical rejection criterion (Chauvenet), discarding samples more than, say, twice the standard deviation.

The histogram is reported for different values of the azimuth: we may clearly observe the peaks at selected values of the phase derivative or group delay, showing the existence of a "main value" for the slope of the phase curve at each specified azimuth (the mean values in the histograms of fig.5).

The proposed method instead than relying on a guess of the *right* wrapping values, relies on a global fit against the shape of the phase response; it actually reveals to be extremely efficient, yielding the satisfactory results reported later.

3 EXTRACTION OF THE AZIMUTH ANGLES

After the measurement of the cues, at each position in the azimuth grid for which HRTFs were computed, we evaluate the weighted error function:

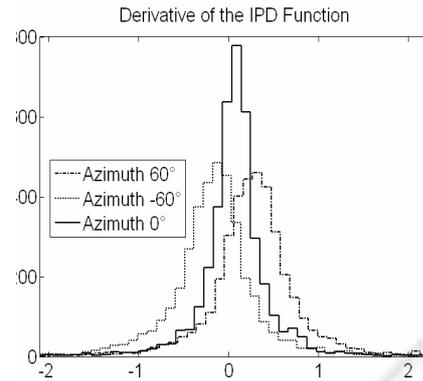


Figure 5: Histogram of point-by-point IPD derivative.

$$S_{IPD}(\theta_i, \omega_k) = \left[\sqrt{(IPD_h(\theta_i, \omega_k) - IPD_m(\omega))^2} \right] \cdot W(\omega_k) \quad (5)$$

Same formula holds for the calculation of $S_{ILD}(\theta_i, \omega_k)$. The weight W is obtained from the bin-aural spectra and has the purpose to give larger weight to those bins in the spectrum where energy is concentrated and where SNR is higher; on the opposite side, in frequency ranges where the signal has low energy, the collected information is to be ascribed mostly to noise and reverberation yielding therefore erroneous and random information on the phase and amplitude content (see fig.2).

This choice, on the ground of the above consideration, may be regarded as a counterpart of the weight used in the GCC method for the evaluation of time differences. In the case of the determination of the Cross Correlation in a generalized way, in order to select bins carrying uncorrupted information we perform proper filtering, say PHAT, ROTH, SCOT or others (see (Knapp and Carter (1976)) for detailed discussion); in our case, where mostly phase of the bins is used, proper selection is performed just by scaling errors in the ILD and IPD by means of weighting with the amplitude of the source signal: best evaluation of this amplitude is just the amplitude of the received signal (see lower part of fig.2). In our experiment we use successfully the following analytical expression for W computed at discrete bins:

$$W[k] = \frac{1}{2} \left(\frac{|X_r[k]|}{\max_j |X_r[j]|} + \frac{|X_l[k]|}{\max_j |X_l[j]|} \right)$$

but different weighting laws perform as well.

The azimuth angle is the angle that minimizes the norm of weighted errors for both parameters in the following way:

$$\theta_{IPD} = \left\{ \theta_j : \|S_{IPD}(\theta_j, \omega_k)\| = \min_i \{\|S_{IPD}(\theta_i, \omega_k)\|\} \right\}$$

$$\theta_{ILD} = \left\{ \theta_j : \|S_{ILD}(\theta_j, \omega_k)\| = \min_i \{\|S_{ILD}(\theta_i, \omega_k)\|\} \right\}$$

4 EXPERIMENTS AND RESULTS

Experiments previously conducted by means of a software simulator (for experimental and software code detail see (Santangelo (2006))) using HRTF from the CIPIC Database ((Algazi, D uda, Thompson and Avendano 2001)) have been also performed by means of a platform consisting of a robotic head on a rotating table (shown in fig.6) and related audio hardware. As sensors at the ears we used two TCM110 electret condenser Tie-Clip microphones by AV-JEFE. The signals were acquired by means of the FirePod, a 24bit 96KHz firewire recording interface by PreSonus.



Figure 6: The platform used for the experiments.

The transfer functions of the robotic head were acquired in a noisy environment (up to 35dB SNR) with a purposely developed software based on a swept sine technique (as shown in (Berkout, de Vries and Boone, 1980), (Farina, 2000) and (Santangelo (2006))).

By means of the rotating table we swept the whole range of positions of the head acquiring measurements for the verification. Results of this measurements are reported in fig. 7 and fig. 8 in the form of histograms of the detected position for one hundred test at each of the angular position of the complete turn; the performance of the proposed algorithm may be easily evaluated.

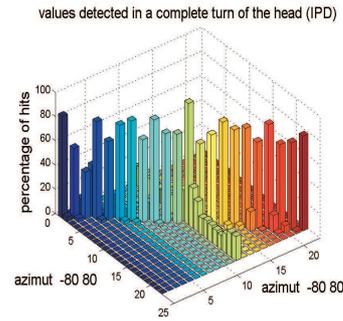


Figure 7: Hit rates for weighted IPD based localization around all grid positions.

Figure 7 shows results in the evaluation of IPD while the figure 8 uses ILD cues. In this latter case results are less robust, especially at extreme positions, where, as well known, angular resolution is poorer.

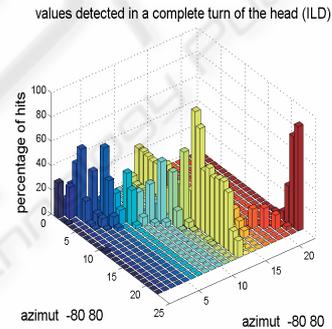


Figure 8: Hit rates for weighted ILD based localization around all grid positions.

The histograms of both figures, show the azimuth values proposed in a complete turn of the head (180). These histograms normalized to 100, as far as regards the bars related to the true positions taken during the experiment (the positions on the -80 80 diagonal) provide also the probability of success in the identification (*hit rate*); this figure in most cases is very close to 100 percent; we must moreover take into account the circumstance that information on angular position taken by considering IPD only may be confirmed by means of the evaluation based on ILD and finally integrated over time by means of a running evaluation, based on STFT: the resulting figures appear therefore to be very satisfactory.

Results, as expected, appear to be more precise at positions close to zero (front positions) and provide higher hit rates while using the IPD cue instead of ILD. The experiments reported in the above figures were conducted using 100 time slots for the duration of 50ms each, taken from a collection of five differ-

ent kind of sounds: male voice, female voice, boys, white noise and a telephone tone, thus providing both wideband and narrowband features.

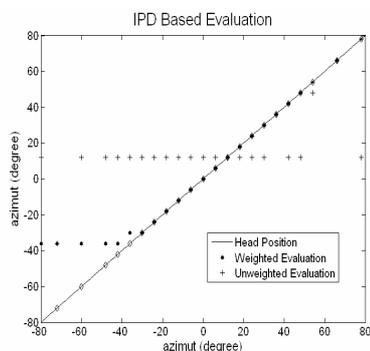


Figure 9: Localization of a narrowband signal. Results are shown for weighted ILD (stars) weighted IPD (diamonds) and unweighted IPD (crosses).

In fig. 9 finally we report results of a narrowband sound localization obtained under the same noise and reverberation conditions by means of the weighted and non weighted table look up methods. It is clear from the diagram that, for all azimuth positions the proposed weighting outperforms the straight look-up method which, while it works in a satisfactory way in simulation by means for example of the CIPIC database (Algazi, D uda, Thompson and Avendano 2001), actually delivers very poor results and high miss rates in the real world conditions.

As expected and as clearly shown in this figure, improvement in performance is greater in the case of narrowband and monochromatic sounds. It is in these cases that, using prevalingly information from bins where the signal shows more energy, exhibiting therefore higher SNR, allows drastically improved performance and provide the confidence that the proposed method appear to be a good candidate for real world performance.

5 CONCLUSIONS

The proposed method seems to outperform the basic table lookup method of which it may be regarded as an extension, compensating for noise and reverberation in real world environments: in the paper we reported the experimental evidence of this. For its promising features the method was chosen for further experiments on a real robot architecture (platform PI-ONEER 3-DX8) on which we are porting the method for real time operation together with an algorithm for face recognition and identification in a multisensory

environment. On this we will report shortly.

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