### ELECTRICAL RELIABILITY OF Cu/Sn MICRO-BUMP IN WAFER LEVEL PACKAGING FOR BioMEMS DEVICES

Myeong-Hyeok Jeong, Jae-Won Kim, Byung-Hyun Kwak, Young-Bae Park School of Materials Science & Engineering, Andong National University, Andong, 760-749, Korea

Byoung-Joon Kim, Young-Chang Joo

Department of Materials Science & Engineering, Seoul National University, Seoul, 151-744, Korea

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Abstract: The electrical reliability of Cu/Sn micro-bump in wafer level packaging for advanced BioMEMS devices applications were systematically investigated during current stressing condition. After bump bonding, Cu<sub>3</sub>Sn and Cu<sub>6</sub>Sn<sub>5</sub> intermetallic phases were observed, and Cu<sub>3</sub>Sn formed and grew at Cu pillar/Cu<sub>6</sub>Sn<sub>5</sub> interface with increasing annealing and current stressing time. The kinetics of intermetallic compound growth changed when all Sn in Cu/Sn micro-bump was exhausted. The complete consumption time of Sn phase in electromigration condition was faster than that in annealing condition. Under current stressing condition, intermetallic compound growth was significantly enhanced by current stressing where the growth rate follows a linear relationship with stressing time.

### **1 INTRODUCTION**

Through-Si-via technology using flip-chip solder bump has recently been investigated in high performance wafer level packaging for advanced BioMEMS device packaging (Chiang, Lee, Lee, and Chen, 2006). This technology assists in the achievement performance high of and miniaturization because the chip and the substrate are directly connected to solder bumps. As the integration of devices increased, the size of solder bump in wafer level packaging became smaller with fine pitch. And increase of current density due to miniaturization of solder bump size with fine pitch causes serious reliability issues of wafer level packaging for advanced BioMEMS applications. The solder bumps become spherical to minimize the surface energy during reflow process (Rao, Tay, Kripseph, Lim, and Yoon, 2004). Bump bridging is caused by the shape of solder in miniaturized electronics. It is limited to applications with a fine pitch below 100 um. Therefore, a new shape for the bump structure is necessary to address this limitation. Cu/Sn micro-bumps are known to be one of the most promising candidates for the fine pitch interconnection materials in wafer level packaging because they do not cause bump bridging between adjacent bumps and uniform current distribution

(Son, Jung, Park, and Paik, 2008). Electrical reliability issues can also be solved with this structure because Cu pillars have superior electric conductivity. At the interface between Cu and solder, Cu6Sn5 and Cu3Sn are formed by the reaction of Cu and Sn, and Kirkendall void is grown (Tu, Mayer, Feldman, 1992). Additionally, the high concentration of Sn in Pb-free solder induces more excessive growth of intermetallic compounds (IMCs) than eutectic SnPb solder (Lee, Zhang, Wong, Tan, and Hadikusuma, 2006). IMCs growth and Kirkendall void formation are important reliability issues of wafer level packaging for advanced BioMEMS devices because IMCs is brittle and has higher resistivity than solder or Cu, which results from the difference in the intrinsic diffusivities of Cu and Sn, in solder joints severely deteriorate the mechanical strength of the joints. The mechanical reliability of solder joints is sensitive to the solder reaction and the microstructure of the solder. Therefore, to ensure the bonding reliability of wafer level packaging for advanced BioMEMS devices, a deep understanding of the IMC growth between Cu and solder is necessary. Many researchers have studied IMCs formation and the growth between Cu and solder in solder bumps and thin film structures (Chao, Chae, Zhang, Lu, Im, and Ho, 2007); but the IMCs growth behaviours in

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Cu/Sn micro-bumps have not been studied systematically. Moreover, under electric current stressing, the IMCs growth is accelerated by the influence of by the electron wind force (Tu, Mayer, and Feldman, 1992, Lee, Zhang, Wong, Tan, and Hadikusuma, 2006, Chao, Chae, Zhang, Lu, Im, and Ho, 2007). Because the current density of Cu/Sn micro-bump is high due to its small size, it is important to understand this behaviour. In this paper, the IMCs growth behaviours in Cu/Sn micro-bumps during simple annealing and under current stress condition was studied systematically using in-situ scanning electron microscope (SEM) observations. IMC growth behaviour of the same sample could be observed in detail by in-situ method which enables us to observe IMCs growth as a function of time in Cu/Sn micro-bumps.

### 2 EXPERIMENT

The schematic and SEM image of the Cu/Sn microbump were shown in Fig. 1. The pad on the Si chip was sputtered with a 2-µm-thick Al film. An Al line provided the electrical path on the Si chip side. A Cu pillar and pure Sn were formed with thicknesses of 40 µm and 1 µm, respectively, on the Al pad using an electroplating process. The thickness and diameter of the Cu/Sn micro-bump were 40 µm and 80 µm, respectively. Pure Sn solders at both the chip and chip were directly interconnected during the bonding process. The bonding was followed by a reflow process with the peak reflow temperature fixed at  $280^{\circ}$ C. The bonding time and load were 7 s and 35 N, respectively. Just after bonding, all samples have similar Sn thicknesses between 1.5 µm and 2 µm. The samples were cross-sectioned with sandpaper after the reflow. To investigate the interfacial microstructure evolution and IMC growth in Cu/Sn micro-bump, in-situ annealing tests were performed via SEM at temperatures of 125°C. And, electromigration test from effect of temperature during current stressing were performed condition with current density of  $3.6 \times 10^4$  A/cm<sup>2</sup> at 125 °C. The temperature of the sample was kept at  $125^{\circ}$ °C by attaching thermo-couple on Si chip. IMC growth was observed at every 20~40 hours. IMC growths at applying various current densities were observed by in-situ as well. The evolution of each interfacial microstructure and the IMC growth of Cu/Sn microbumps were analyzed using SEM in back-scattered electron (BSE) mode and energy-dispersive x-ray spectroscopy (EDS). IMC thickness was measured from the IMC layers at both the chip and substrate

sides. The Cu-Sn IMC thickness was quantified with an image analyzer where the IMC thickness was defined by dividing the area of the IMC by the interface length.



Figure 1: (a) Schematic diagram and (b) SEM image of Cu/Sn micro-bump structure.

### **3 RESULTS AND DISCUSSION**

# 3.1 Interfacial Reaction Characteristics during Annealing

To observe the evolution of the interfacial microstructure and the growth of Cu-Sn IMCs on Cu/Sn micro-bumps with annealing temperature and time, BSE images were taken of cross-sectioned Cu/Sn micro-bump annealed at  $125^{\circ}$ C, as shown in Fig. 2. The SEM and EDS results suggest that only Cu<sub>6</sub>Sn<sub>5</sub> was observed at the Cu pillar/Sn interfaces, and micro-voids exist in the Sn phase after reflow. The micro-voids seem to originate from the flip-chip bonding process, and they arise from the defects in the samples. Kirkendall voids were observed at the Cu pillar/Cu<sub>3</sub>Sn interface as well as within the Cu<sub>3</sub>Sn layer. It has been reported that the Kirkendall void formation mechanism is ascribed to the different diffusivities of Cu and Sn (Tu, Mayer, and Feldman, 1992). Cu<sub>3</sub>Sn formed and grew at the Cu pillar/Cu<sub>6</sub>Sn<sub>5</sub> interface with increasing annealing

time. It has been reported that the Cu<sub>6</sub>Sn<sub>5</sub> and Cu<sub>3</sub>Sn phases are generally formed at the Cu/Sn interface during the reaction between Cu and Sn. Cu<sub>3</sub>Sn layer on both interfaces have grown up with the similar thicknesses. The Sn phase was not observed at the Cu/Sn micro-bump interface after 60 h at 125. Fig. 3 shows the thickness of the IMCs as a function of the square root of the annealing time at 125°C. The growth of the IMC followed a linear relationship with the square root of the annealing time. This implies that the growth of the total IMC was controlled by a diffusion mechanism. To understand the variation of IMC growth slopes at 125°C, the IMC thicknesses of the Cu<sub>6</sub>Sn<sub>5</sub> and Cu<sub>3</sub>Sn phases as a function of the square root of the annealing time at 125℃. The Cu<sub>6</sub>Sn<sub>5</sub> and Cu<sub>3</sub>Sn phases linearly increased together before 60 h at  $125^{\circ}$ C, and then the Cu<sub>6</sub>Sn<sub>5</sub> phase rapidly decreased from initial at 125°C. The Cu<sub>3</sub>Sn growth rate was also faster than the Cu<sub>6</sub>Sn<sub>5</sub> growth rate compared with the Cu-Sn reaction system of a conventional solder bump structure, which is a Cu-limited system. This seems to arise from the Cu/Sn micro-bump structure, which is a Sn-limited system.



Figure 2: BSE micrographs of the enlarged crosssectioned Cu/Sn micro-bump during annealing at 125°C.



Figure 3: Intermetallic compound layer thickness with annealing time at 125°C.

## 3.2 Interfacial Reaction Characteristics during Electric Current Stressing

Electromigration test was performed with current density of  $3.6 \times 10^4$  A/cm<sup>2</sup> at 125 °C. In order to obtain the growth kinetics of IMCs in Cu/Sn microbump, in-situ BSE images were taken from crosssectioned Cu/Sn micro-bump during current stressing as shown in Fig. 4. The microstructural observation results suggest that only Cu<sub>6</sub>Sn<sub>5</sub> was observed at the Cu pillar/Sn interfaces and a few micro-voids exist in the Sn phase just after reflow. During current stressing, Cu<sub>3</sub>Sn phase grows at Cu/Cu<sub>6</sub>Sn<sub>5</sub> interfaces and pure Sn phase disappears after 40 h where the electron wind force seems to enhance the IMC formation reaction between Cu and Sn (Lee, Zhang, Wong, Tan, and Hadikusuma, 2006, Chao, Chae, Zhang, Lu, Im, and Ho, 2007). Higher temperature enhances the interfacial reaction which leads to earlier consumption of pure Sn phase. Therefore, the temperature as well as the electric current accelerates the IMC reaction rate between Cu and Sn. Figure 5 shows the IMC growth behavior over current stressing time. It is noticeable that the IMC thickness increases linearly with stressing. This is closely related to different reaction kinetics of electromigration compared to pure annealing. We believe that there are competitions between diffusion inside IMCs and chemical reaction at Cu/Sn interface. After characteristic stressing time, the IMC growth slope has sharply decreased, which can be seen clearly from magnified BSE images in Fig. 4. Different bump structure and material systems might lead to different reaction limiting systems.

#### **4** CONCLUSIONS

The IMCs growths behaviors and electrical reliability of Cu/Sn micro-bump in wafer level

packaging for advanced BioMEMS devices applications were systematically investigated by insitu SEM observation method. During current stressing condition, IMC thickness increased linearly with stressing time. It was observed that Cu<sub>3</sub>Sn growth rate was larger than that of Cu<sub>6</sub>Sn<sub>5</sub>, which is opposite result observed in conventional solder bump. After the complete Sn exhaustion in the bump,



Figure 4: BSE micrographs of the cross-sectioned Cu/Sn micro-bump during current stressing at  $3.6 \times 10^4$  A/cm<sup>2</sup> and 125°C.



Figure 5: Intermetallic compound layer thickness with current stressing time at  $125^{\circ}$ C and  $3.6 \times 10^4$  A/cm<sup>2</sup>.

 $Cu_6Sn_5$  thickness became to decrease and  $Cu_3Sn$  grew faster. When current applied in Cu/Sn microbump, IMC grew faster than annealing condition, and the transition time of IMC growth was shortened, and the transition time showed inverse proportional to current density. Electrical Lifetime should be correlated to this microstructural evolution during current stressing.

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