GRASP FEASIBILITY COMPUTATION BASED ON CASCADING FILTERS. APPLICATION TO A THREE FINGERED GRIPPER

Cesar Fernandez, M. Asuncion Vicente, Oscar Reinoso, Luis Paya, Rafael Puerto Industrial Systems Engineering Department. Miguel Hernandez University Av. Universidad s/n. 03202 Elche (Alicante), Spain.

Keywords: Robot grasping, inverse kinematics, collision detection, optimization.

A simple, yet effective approach to grasp feasibility analysis is presented. The goal is to reduce the computa-Abstract: tional complexity of such process, whose complexity makes the detection of all feasible grasps for a certain object unavoidable in most occasions. The approach is based on cascading filters of increasing complexity. First, trivial filters are applied to all the grasp examples, thus rejecting all clearly unfeasible grasps with a small computational effort. Then, more complex filters are applied to a reduced number of grasps and, at the end, the full kinematics and collision detection analysis is only performed with a small subset of the grasps. An example application is presented, where the goal is to detect all the possible 2D grasps of a certain object with an articulated three-fingered hand attached to a scara robot. The vertical axis is decoupled, thus resulting in a highly redundant 7 DOF planar device. Simulation results are presented, where the reduction in computational complexity is evaluated in terms of the number of floating point operations required. Such reduction can be as high as 97% of the original computation time. An experimental setup has also been developed, with an industrial scara robot and a specifically designed articulated three-fingered gripper. The gripper has pneumatically actuated opening and closing of the fingers and electrically actuated abduction of the articulated fingers. In such experimental setup, the cascading filters approach shows a good behavior. Besides, the proposed system can be easily adapted to different robot arms and hands.

1 INTRODUCTION

The goal of a robot grasp synthesis algorithm is to select the best grasp for a certain object, given a robot arm and hand. The number of different grasps that have to be analyzed can be extremely high, particularly when multifingered grippers are used. In a generic situation, a grasp is defined as a set of n contact points on the surface of the object, where n is the number of gripper fingers. Let us suppose that the surface of the object can be defined to a certain resolution by z 3D points. In such situation, there are $\binom{z}{n}$ possible sets of contact points. If the gripper is not symmetric, finger assignment is also relevant, so each set represents n! different grasps, and the total number of grasps can be expressed as N_G in Eq. 1

$$N_G = \binom{z}{n} \cdot n! = \frac{z!}{(z-n)!} \tag{1}$$

Each of the N_G possible grasps has to be analyzed for feasibility. There are two main aspects that need to be considered: first, the kinematics of robot arm and gripper; and second, the existence of collisions.

Concerning the first aspect, the goal is to detect whether the set of n points is reachable or not taking into account the root arm and gripper kinematics: i.e. the goal is to solve the inverse kinematics. In the general situation, there is a high level of redundancy, and the computation of the inverse kinematics is thus very expensive. Only very simple grasping devices like two jaw parallel grippers are nonredundant. Apart from that, there are several particularities in grasp kinematics. First, there are multiple end effectors, one per gripper finger, which are coupled (some of the joints are common for several fingers); and second, desired configurations (end effector poses) are not strict in terms of orientation. This remark is shown in figure 1, where two different sets of end effector orientations reaching the same contact points have to be considered valid and capable of performing the grasp.

As it has been mentioned before, there is a second aspect to be considered: the existence of colli-



Figure 1: Orientation is not a strict restriction when computing the inverse kinematics of a grasp defined by n contact points.

sions. Even if the robot arm and gripper kinematics allows to reach a certain set of n contact points, the final configuration could produce collisions between the object and the robot links (only the final configuration is taken into account as the problem of the path followed by the robot gripper from the initial configuration is not addressed in this paper). The detection of the possible collisions is also a computationally expensive problem.

In the present paper, a simple yet effective computational reduction technique is presented. Such technique is specifically designed for robot grasping, and takes into account all the particularities of such problem.

The paper is structured as follows: section 2 describes the previous approaches to kinematic computation in the presence of redundancy and to collision detection; and outlines their limitations for a robot grasp application. Section 3 presents the proposed approach; and section 4 its application to a certain grasp environment. Sections 5 and 6 present the results obtained both in simulation and in a real experimental setup. Finally, some conclusions are drawn on section 7.

2 PREVIOUS APPROACHES TO FEASIBILITY STUDY

Concerning the computation of the inverse kinematics in the presence of redundancy, multiple solutions can be found in the literature. The easiest approach is to add constraints for the redundant DOF; i.e. to held fixed a certain joint or to establish some fixed relationships between different joints. However, these solutions are not valid when the goal is feasibility computation: some of the available DOF are not exploited, and a grasp could be incorrectly classified as unfeasible. Other approaches are based on the use of iterative methods to approximate a good solution, normally based on the Jacobian matrix J. In a general case, when there are multiple end effectors (e.g. grasping devices) the Jacobian matrix is defined as in Eq. 2, where p_i denotes the i-th end effector position (depending on the applications, p_i can represent both the end effector positions and orientations) and q_j denotes the j-th robot joint.

$$J(Q) = \left(\frac{\partial p_i}{\partial q_j}\right)_{i,j} \tag{2}$$

Inverse kinematics resolution based on the Jacobian matrix can be accomplished in many different ways: the Jacobian transpose method (Balestrino et al., 1984)(Wolovich and Elliot, 1984), the Jacobian pseudoinverse or null-space method (Baillieul, 1985), the damped least squares method (Nakamura, 1986), etc. However, these approaches are devoted to find a solution to the inverse kinematics and not to simply detect whether a solution exists; in this way, their computational requirements could be reduced.

Other redundancy resolution methods are based on parametric modelling rather than in the Jacobian matrix. In (Dordevic et al., 2004), an approach based on human motor control theories is presented. A taxonomy of robot motions is generated and, for each motion example, the joint values are computed in an off-line step called skill acquisition. When the robot is requested to perform a certain motion, function approximators are used to interpolate the joint values corresponding to the desired motion from the available skills. The main advantage of this method is its low on-line computational complexity; but it is not valid to detect the feasibility of a certain grasp. First, it is devoted to robot motions; and second, a grasp could be classified as unfeasible even if it could be feasible using a configuration different to that of the stored skills.

Concerning the collision detection problem, multiple algorithms have also been developed. When the goal is collision free path planning, the configuration space (Lozano-Perez, 1983) is commonly used; however, the present paper is focused on the detection of the collisions for the final gripper configuration, and not on the path followed to reach such configuration. When the goal is the detection of collisions in a static configuration, most algorithms are based on the representation of all the objects that could collide (robot links, object to be grasped and maybe surrounding obstacles) as sets of planar faces. The resolution used for such representation is a key factor in obtaining a good compromise between computational load and accuracy of the results. A survey on collision detection techniques can be found in (Jimenez et al., 2001). There are multiple available optimized software packages, like I-COLLIDE (Lin, 1993), RAPID

(Gottschalk et al., 1996), V-COLLIDE (Hudson et al., 1997), QUICK-CD (Klosowski, 1998), etc. In these software packages, the goal is to detect precisely the contact point or contact areas of a collision. Such information is not needed for feasibility computation; it is just required to know whether there is a collision or not.

3 PROPOSED APPROACH

The proposed approach is focused on feasibility computation and not on computing the full inverse kinematics or detecting precisely the contact points of a collision. In order to reduce the computational load, cascading filters of increasing complexity are applied.

First, trivial filters are applied to all the grasp examples, thus rejecting all clearly unfeasible grasps with a small computational effort. These trivial filters compute absolute and relative distances for the n contact points of the grasps and check whether the maximum values, minimum values and ratios of such distances fall within the valid ranges of robot arm and gripper.

Once this trivial filters have been applied and part of the grasp candidates have been discarded, more complex filters are applied to the remaining grasps. This slightly more complex filters compute angular measurements and trivial collision detection criteria in order to reduce even more the number of grasp candidates. At this second step, the computational effort required to test each grasp is higher but the number of grasps to be checked is smaller as some of the candidates were already filtered in the first step.

The complexity of the applied filters is increased at each step, as the number of grasps examples where the filters have to be applied is reduced. Finally, the most complex filters (full kinematics analysis and collision detection) are performed only in a very reduced subset of examples. Figure 2 shows the cascading filters structure.



Figure 2: Cascading filters: complexity increases as the number of checks to be performed decreases.

The number of filters used is a key factor in the reduction of complexity. Apparently, increasing the number of filters should always result in a computational load decrease, provided the filters are chosen wisely. However, the valid grasps (the ones not discarded) have to be evaluated with all the filters. If the number of filters is too high, computational load could be increased instead: a compromise is required.

The cascading filters approach is particularly suited to grasping applications, where multiple grasp candidates have to be evaluated in order to choose the best one. Each of the filters used have to be specific to a certain robot arm and gripper, but the methodology can be applied in general terms to all situations: the most simple filters deal with distance measurements; at a higher complexity level angular measurements are considered; then trivial collision detection is performed; and finally the full tests are carried out.

These full tests have to be slightly different to those proposed in the literature, as the only requirement is to detect whether a valid solution exist. Ad-hoc filters should be developed depending on the application.

4 APPLICATION TO A THREE-FINGERED GRIPPER

4.1 Definition of the example application

The proposed approach has been applied to a robot grasping environment. The goal is to detect all the possible 2D grasps (planar grasps) that can be performed with an articulated three-fingered gripper attached to a scara robot. The problem is analyzed in 2D so the vertical axis of the scara robot is decoupled. Figure 3 shows the planar kinematics of arm and gripper.



Figure 3: Planar kinematics of the example application.

The system has a total of seven planar DOF, which are clearly marked in the figure: three of them translational (opening and closing of the fingers, which are independent) and one rotational (abduction of the two articulated fingers, which are coupled). There is a high redundancy, as a certain set of three contact points can be reached with multiple configurations of robot arm and gripper.

4.2 Selected filters

The filters used for the example application are described in the next paragraphs. A total of five filters

have been defined:

- 1. The first filter measures the distance from the midpoint of the three contact points to the robot origin. Extremely large or extremely small distances result in unfeasible grasps.
- 2. The second filter measures point to point distances between the three contact points, and computes the maximum value, the minimum value, the sum of distances and the difference between maximum and minimum values. All these measures have to fall within the gripper range in order for the grasp to be accepted.
- 3. The third filter measures the angle between the surface normals at the three contact points: normals that are too close to be parallel will be kinematically unfeasible or will result in a collision. A threshold of 45 degrees is used.
- 4. The fourth filter computes the expected angle between the surface normals and the finger action line. There are three possible finger assignments for this gripper (three different ways of assigning contact points to robot fingers), and at least one of the assignments must result in valid values for this angle: a range of \pm 45 degrees is allowed.
- 5. Finally, the fifth filter computes a full kinematic analysis and collision detection. As there is redundancy, no closed solution for the inverse kinematics can be found. To solve this problem, the range of motion of one of the joints (abduction of the two articulated fingers) is discretized to a fixed resolution (100 values) and an analysis of kinematics feasibility is performed for each abduction value. The collision detection needs to be performed simultaneously: as the fingers are supposed to have planar surfaces, the expected contact points may be slightly different to the real ones. In order to take this effect into account, the previously computed finger strokes are modified in order to avoid interferences between fingers and object. If the finger strokes are within valid ranges after the modification, the grasp is considered to be feasible. Even though the computational load of this filter is not very high, it is much more complex than the previous filters.

5 RESULTS IN SIMULATION

In order to check the validity of the proposed approach, a Matlab simulation environment has been developed. This environment allows to represent any 2D robot arm and hand; for the experimental comparison, the scara robot and the three-fingered gripper described in section 4.1 are chosen. A database of 24 synthetic objects has been defined, and a scale factor

has been applied to increase the variability of the examples: every object can have five different sizes, thus resulting in a total of 120 different contours. Such database is shown in figure 4.



Figure 4: Synthetic objects defined for the simulation environment.

During a simulation, a randomly chosen object is presented in a random pose, which can be within reach of the robot arm or not. The object contour is discretized using an adjustable resolution and all the feasible grasps are computed an displayed. Figures 5 and 6 show the process. Both a detailed view of the object and a general view of its relative pose with respect to the robot arm are displayed (bottom right window of the image).



Figure 5: Simulation setup, first step: an object is presented in a random pose and its contour is discretized.

This simulation setup has also been used to test a grasp synthesis algorithm (Fernandez et al., 2004)



Figure 6: Simulation setup, second step: all the feasible grasps are computed and displayed. Resolution has been reduced in order to obtain a better visualization.

which, provided the feasible grasps have been computed, selects the best one by similarity to grasp examples provided by the user and performs such grasp, displaying the robot arm and gripper movements. However, this paper is focused on the previous step: the computation of the feasible grasps.

Such computation is performed following the cascading filters approach presented in previous sections. Figure 7 shows the behavior of the system over some example objects belonging to the database: the number of grasps to be checked for feasibility gets smaller as the filter complexity increases. The goal has been achieved, as the relatively complex fifth filter is only evaluated in a small subset of grasps.



Figure 7: Simulation results: number of grasps remaining after applying each filter.



Figure 8: Simulation results: number of floating point operations required to perform each feasibility computation.

Concerning the computational complexity associated with each filter, figure 8 shows the number of floating point operations required to perform each filter computation. A logarithmic scale is used in the y axis in order to be able to represent the high differences in computational load between the different filters; particularly, the fifth filter is much more complex than the others.

The combination of the results shown in figures 7 and 8 gives the total computational load. Table 1 compares these results against the computational load associated with a direct application of the most complex filter (full kinematics and collision analysis) to all the possible grasps. It becomes clear that there are high reductions in complexity, that range from 71% to 98% (i.e. the proposed approach requires only the 2% of the original computing time for certain objects).

Table 1: Comparison of computational complexity in terms of floating point operations required to compute all the feasible grasps for some example objects.

Object	Cascading	All tests	Reduction
1	$4.72 \cdot 10^{6}$	$8.56 \cdot 10^{7}$	94.5%
2	$8.03 \cdot 10^{6}$	$4.39\cdot 10^7$	81.7%
3	$4.92 \cdot 10^{6}$	$7.72 \cdot 10^{7}$	93.6%
4	$1.12 \cdot 10^{7}$	$2.33\cdot 10^8$	95.2%
5	$4.03 \cdot 10^{7}$	$1.43 \cdot 10^{8}$	71.8%
6	$4.59 \cdot 10^{6}$	$2.29 \cdot 10^{8}$	98.0%
7	$9.98 \cdot 10^{6}$	$9.22 \cdot 10^{7}$	89.1%

6 RESULTS IN A EXPERIMENTAL SETUP

A real experimental setup has also been used to check the validity of the approach. An articulated threefingered gripper has been designed and developed specifically for these tests, following the structure of the example application presented in section 4. It allows independent finger strokes, with pneumatically actuated opening and closing; and it has an extra DOF which allows to modify the abduction of the two articulated fingers in the range 0 to 180 degrees. Such abduction is electrically actuated by a DC motor. The result is a highly redundant robot gripper. Figure 9 contains some drawings where the basic design and the range of reachable abduction values is shown; figures 10 and 11 show two images of the real device using different configurations to hold different objects. In these figures, it becomes clear that the gripper has been designed in order to be adaptable to objects of different shapes. The basic structure of the Barret hand (Bar,) has been used as a guideline.



Figure 9: Design of the three-fingered articulated hand and range of abduction values.



Figure 10: Developed gripper: configuration used to hold objects with spherical shape.

The experimental setup includes also a Mitsubishi RH-5AH55 scara robot where the gripper is attached (details about such robot can be found in (Mit,)) and a low cost Creative video camera (Cre,) to detect the contour of the objects to be grasped. Figure 12 shows this environment. The camera is fixed to the robot arm, following an eye-in-hand configuration. To obtain the contour of the objects, a color-based region growing algorithm is used, which grows the back-



Figure 11: Developed gripper: configuration used to hold objects with cylindrical shape.

ground region starting at one the image corners (uniform blue backgrounds and semi-controlled lighting are used for the experiments). Afterwards, a set of 5 consecutive morphological closings are performed in order to smooth the initial contours and discard irrelevant irregularities. All the image processing operations are performed using functions from the OpenCV library (Ope,). The results of the contour extraction process on some example images are shown in figure 13. The system is robust enough to detect the contours of most objects, even when highly reflective surfaces are present.

Once the contours are extracted, they are discretized to a certain resolution and the cascading filters approach is used to detect the feasible grasps. In order to check the behavior of the system, both the contour and the feasible grasps computed are displayed using a Matlab application similar to the one used in the simulation setup. Figures 14 and 15 show an example of contours extracted from a real object, its discretization and the feasible grasps. A certain level of noise is present in the extracted contour, but the results are almost unaffected.



Figure 12: Experimental setup: robot arm and gripper and video camera.



Figure 13: Contours obtained for some example objects.

Finally, some experiments are performed with different objects in order to check the reduction of computational load in the real environment. The same structure used with the simulation setup is followed. Table 2 and figures 16 and 17 show the results obtained in terms of number of grasps kept after each filtering; computational load of each filter in floating point operations; and total computational load . The efficiency of the proposed approach is confirmed as the reduction in computational complexity ranges from 63% to 97%.



Figure 14: Experimental setup, first step: an image is captured, and the object contour is extracted and discretized.



Figure 15: Experimental setup, second step: all the feasible grasps are computed and displayed.

Table 2: Comparison of computational complexity in the experimental setup.

Object	Cascading	All tests	Reduction
1	$4.94 \cdot 10^{6}$	$1.05 \cdot 10^{8}$	95.3%
2	$7.59 \cdot 10^{7}$	$1.11 \cdot 10^{9}$	93.1%
3	$1.04 \cdot 10^{7}$	$3.89 \cdot 10^{8}$	97.3%
4	$2.29 \cdot 10^{8}$	$1.44 \cdot 10^9$	84.1%
5	$4.63 \cdot 10^{6}$	$1.27 \cdot 10^{7}$	63.4%
6	$1.95 \cdot 10^{7}$	$1.83 \cdot 10^{8}$	89.3%
7	$1.79 \cdot 10^{7}$	$1.02 \cdot 10^{8}$	82.5%



Figure 16: Experimental results: number of grasps remaining after applying each filter.



Figure 17: Experimental results: number of floating point operations required to perform each feasibility computation.

7 CONCLUSIONS

Detecting all the feasible grasps for an object, given a certain robot arm and hand, is a computationally expensive and normally unavoidable problem. Previous research in this field is devoted to optimize the resolution of the full inverse kinematics problem or to optimize the detailed detection of collisions.

The approach presented in this paper allows to perform a fast feasibility study for all the possible grasps of a certain object, computing the inverse kinematics and collision detection only in a reduced subset of grasps.

Such approach can be adapted to any robot arm and hand, as it has been shown with an example application.

Experimental results performed both in simulation and on a real environment show that the proposed approach allows high reductions in computational load.

Future work will be devoted to the application of the proposed system in more complex grasping devices (robot hands); and also to consider the existence of collision free paths instead of the static collision detection tests performed at present.

REFERENCES

Barret hand. <http://www.barretttechnology.com>.

Creative. <http://www.creative.com>.

Mitsubishi. < http://global.mitsubishielectric.com/bu/automation>.

Opencv. <http://www.intel.com/research/mrl/research/opencv>.

Baillieul, J. (1985). Kinematic programming alternatives for redundant manipulators. In *Proc. IEEE Int. Conf. on Robotics and Automation*, pages 722–728.

- Balestrino, A., De Maria, G., and Sciavicco, L. (1984). Robust control of robotic manipulators. In *Proceedings of the 9th IFAC World Congress*, volume 5, pages 2435–2440.
- Dordevic, G., Rasic, M., and Shadmehr, R. (2004). Parametric models for motion planning and control in biomimetic robotics. *IEEE Transactions on Robotics*. (in press).
- Fernandez, C., Vicente, M. A., Reinoso, O., and Aracil, R. (2004). A decision tree based approach to grasp synthesis. In Proceedings of the International Conference on Intelligent Manipulation and Grasping, pages 486– 491.
- Gottschalk, S., Lin, M., and Manocha, D. (1996). A hierarchical structure for rapid interference detection. In *Proc. of ACM Siggraph*'96, pages 171–180.
- Hudson, T., Lin, M., Cohen, J., Gottschalk, S., and Manocha, D. (1997). V- collide: Accelerated collision detection for vrml. In *Proc. of VRML Conference*, pages 119–125.
- Jimenez, P., Thomas, F., and Torras, C. (2001). 3d collision detection: a survey. *Computers and Graphics*, 25(2):269–285.
- Klosowski, J. (1998). Efficient Collision Detection for Interactive 3D Graphics and Virtual Environments. PhD thesis, University of New York.
- Lin, M. (1993). Effcient Collision Detection for Animation and Robotics. PhD thesis, University of California.
- Lozano-Perez, T. (1983). Spatial planning: a configuration space approach. *IEEE Transactions on Computers*, 32(2):108–120.
- Nakamura, Y. (1986). Inverse kinematics solutions with singularity robustness for robot manipulator control. *Journal of Dynamic Systems, Measurements and Control*, 108:163–171.
- Wolovich, W. A. and Elliot, H. (1984). A computational technique for inverse kinematics. In *Proc. of the 23rd IEEE Conf. on Decision and Control*, pages 1359– 1363.